




**LIFING**

**PIPING**

**Current Release: 3.4**

# OUTLOOK

- What is LIFING
-  LIFING.Life
  - **FEM INTERFACES**
  - **ANALYSIS PROCESS**
  - **IMPLEMENTED ANALYSIS METHODS (TIME DOMAIN)**
  - **FATIGUE BASED ON PSD (FREQUENCY DOMAIN)**
  - **VIRTUAL STRAIN GAUGE**
-  LIFING.Growth
  - **ANALYSIS PROCESS**
  - **IMPLEMENTED ANALYSIS METHODS**
-  QUICK2DFEM
- Technical Information
- References

# WHAT IS LIFING

- LIFING is a software for performing Fatigue and Damage Tolerance (F-DT) FEM based analysis of components.
- LIFING includes the following modules:



## **LIFING.Life**

### **Multiaxial Fatigue analysis**

- Stress and Strain based analysis methods (multiaxial) are implemented
- PSD based fatigue implemented
- Multiple features for post-processing are included, such as Virtual Strain Gauges, to retrieve at any point in the FEM a stress tensor time history



## **LIFING.Growth**

### **Crack Growth analysis**

- 2D and 3D FEM can be solved to extract Stress Intensity Factors (internal FEM solver and mesher; J-Integral calculated at crack tips in 2D FEM where «quarter point elements» are used; M-Integral calculated at crack fronts in 3D FEM where «quarter point elements» are used.
- 3D Solid Mesh Sections can be solved (Stress Intensity Factors are calculated based on Newman-Raju solution corrected with Glinka's Weight Functions using stress distributions automatically extracted at section cuts, or imported from file)
- NASGRO model or  $da/dN$  in tabular format used for integrating Crack Growth Life curve

# WHAT IS LIFING

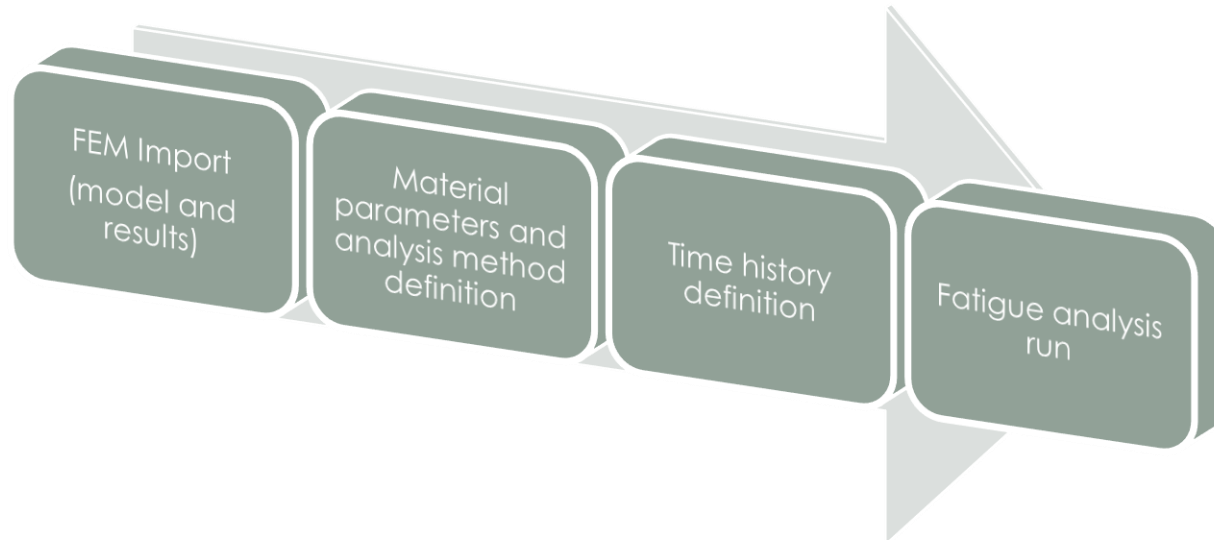


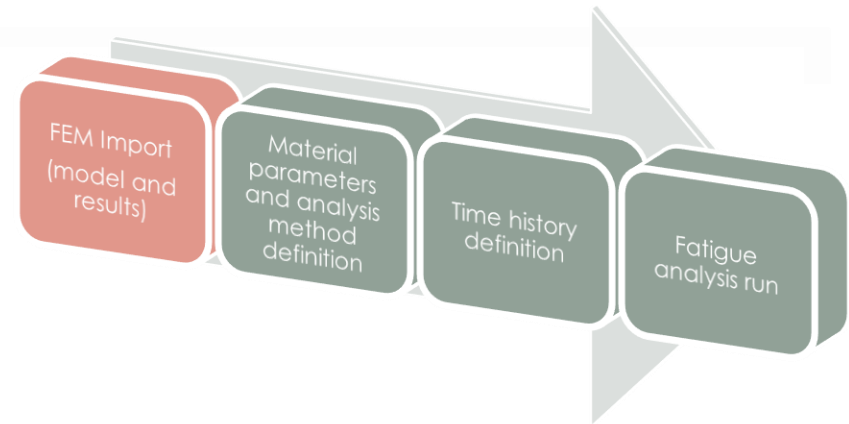
## QUICK2DFEM

- Creation of 2D models on the basis of simple scripts
- 2D FEM Solver
- Creation of 3D models from extrusion of 2D models
- 3D FEM Solver
- Capability to introduce crack fronts and calculate Stress Intensity Factors
- Cost effective to design repairs, assess stress concentration factors, estimate quickly design deviations, ...

# LIFING.Life

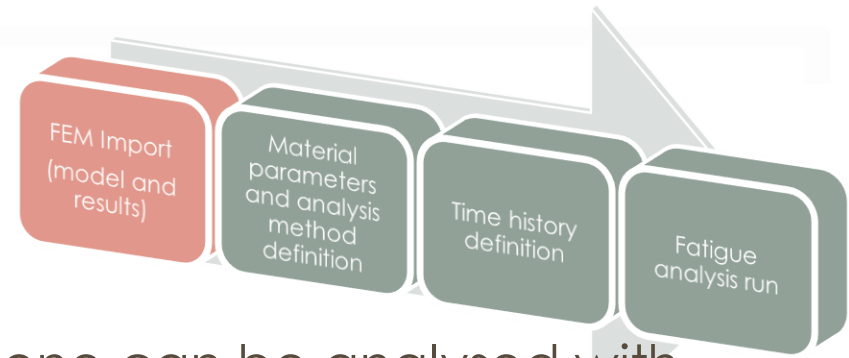
- LIFING calculates fatigue, in general crack initiation, in a FEM component or assembly
- The analysis can be conducted with multiple methods:
  - **Stress based methods**
  - **Strain based methods**
- The workflow:



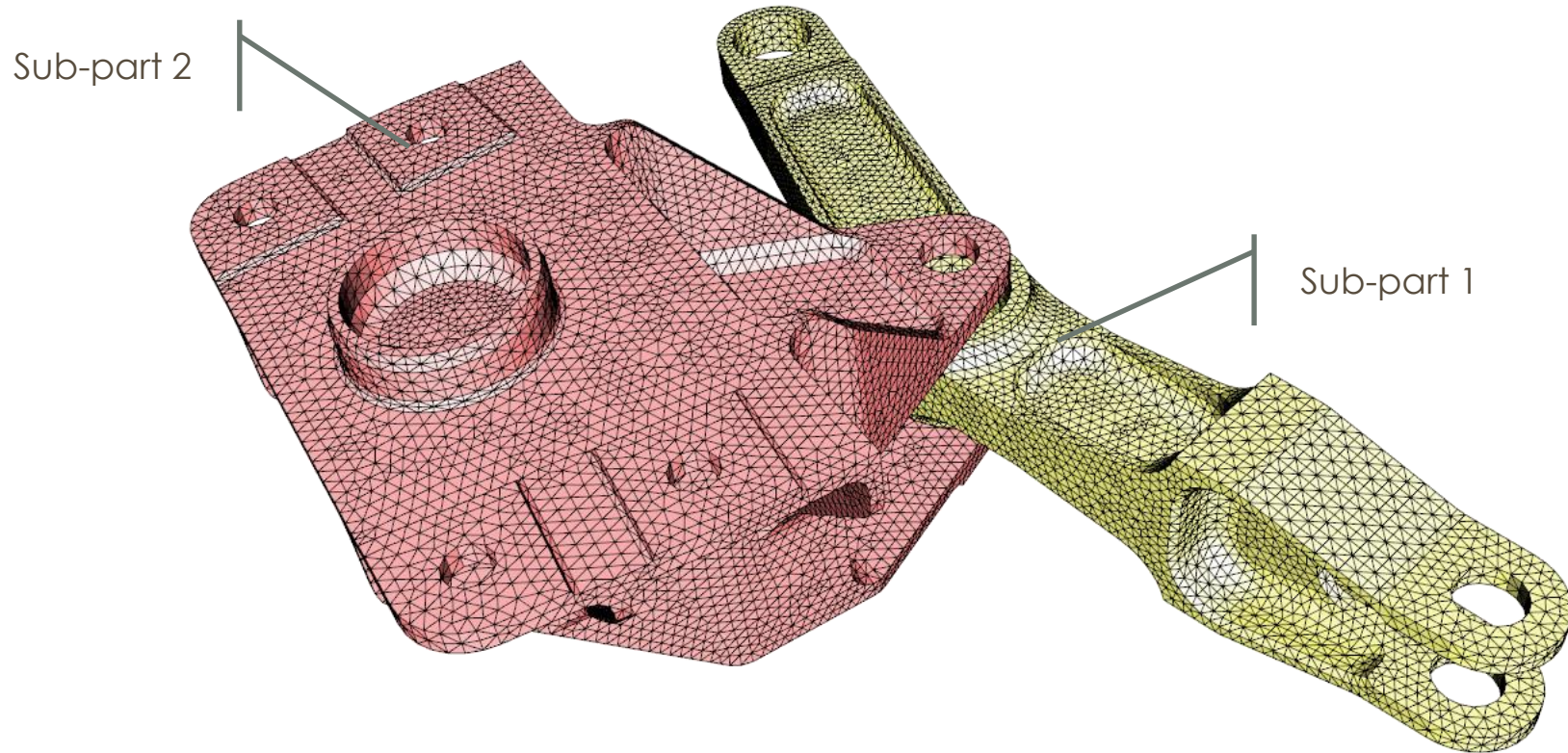


- LIFING includes FEM interfaces for:
  - **NASTRAN, OPTISTRUT**
    - Import of model (ASCII file NASTRAN format) and results files OP2 (binary) and PCH (ASCII) generated by NASTRAN/OPTISTRUT
  - **ANSYS**
    - Import of model (ASCII file ANSYS format) and results files (ASCII) generated by ANSYS (the CDB binary file interface is not available)
  - **ABAQUS, CALCULIX**
    - Import of model (ASCII file ABAQUS/CALCULIX format) and results files FIL (ASCII) generated by ABAQUS and FRD (ASCII) generated by CALCULIX

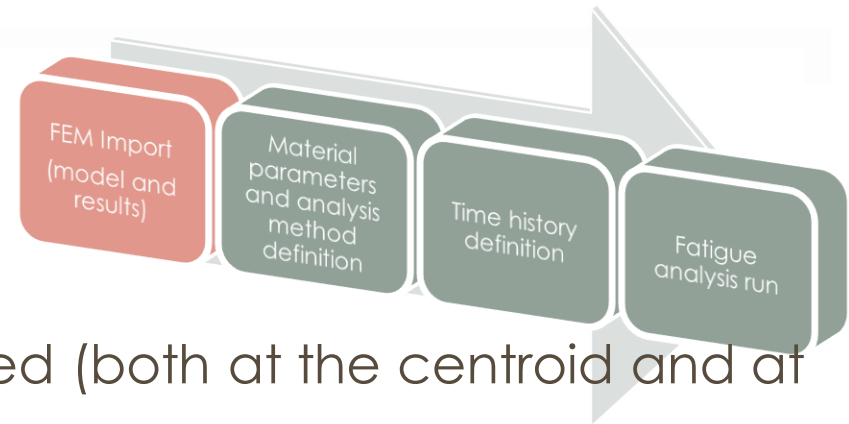




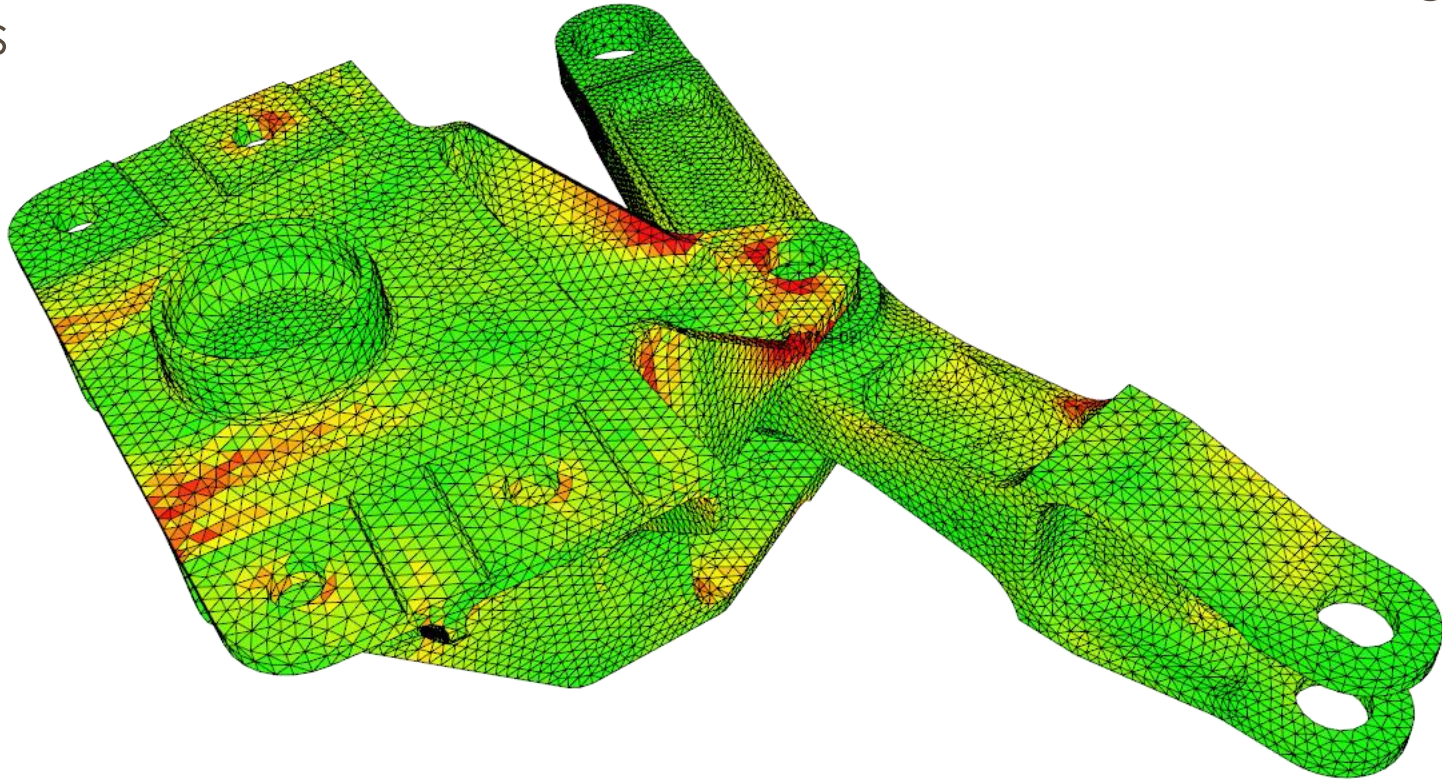
- The FEM can be split in sub-parts (each one can be analysed with different methods and/or parameters, e.g. for accounting local surface treatments)



# LIFING.Life

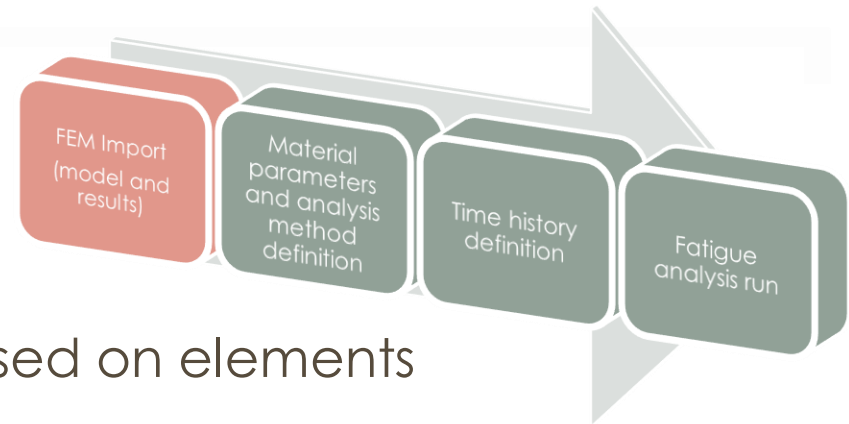


- Elemental stresses can be post-processed (both at the centroid and at the surfaces)
- Only elements and stresses at the surfaces are retained for fatigue analysis

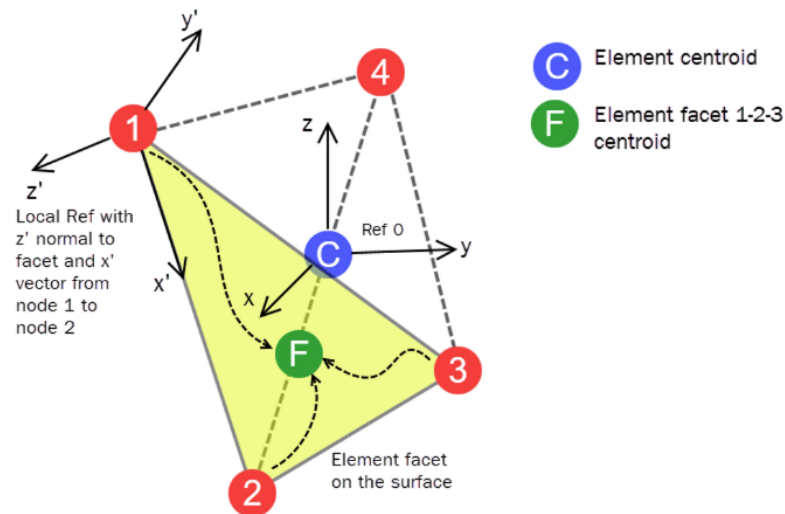




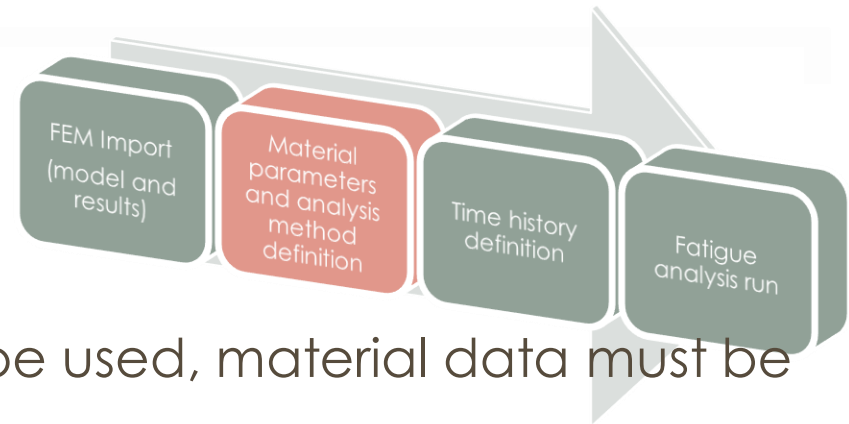
# LIFING.Life



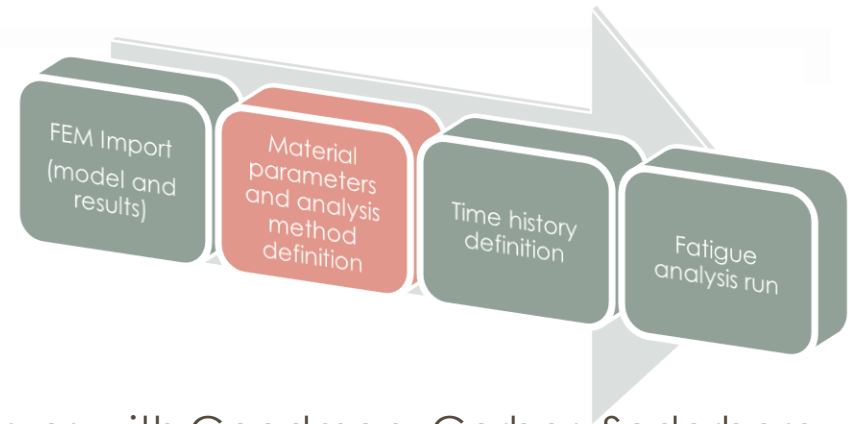
- LIFING.LIFE performs fatigue analysis based on elements
- Stresses at facets are:
  - Either taken from centroidal stresses and rotated to local reference system with  $Z'$  axis perpendicular to the element facet
  - Either derived from nodal stresses (if available in the result file) as shown in the sketch



- Gradient effects can be accounted or stresses can be derived at a critical distance from the surface



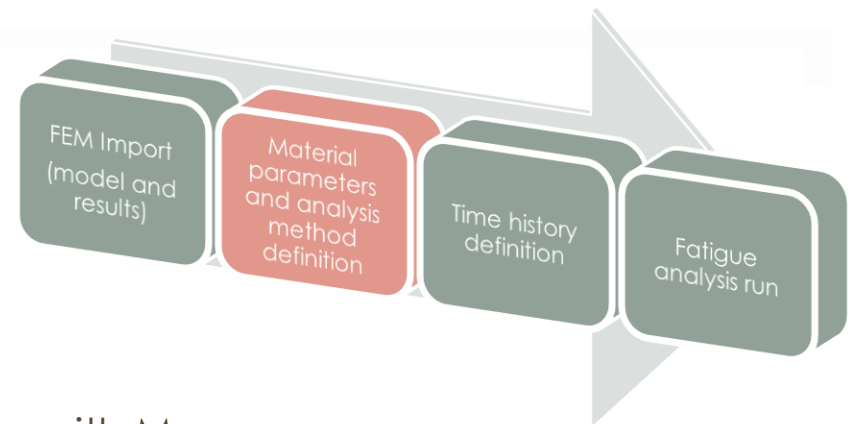
- Depending on the analysis method to be used, material data must be provided
  - S-N curves (generic format or military standard format)
  - Strain-life and cyclic stress-strain curves
- One set of material data and analysis method is assigned to the entire FEM, however different materials and analysis methods can be assigned to the FEM sub-parts
  - If nothing is specified to the Sub-parts, they will be analysed considering the 'global' material data and analysis method, otherwise...
  - ...they will be analysed considering the specified data
- Residual stress conditions can be considered
  - Constant residual stress applied to the entire FEM or differentiated by Sub-Parts
  - Stress offset from a specific static load case



- Stress based methods

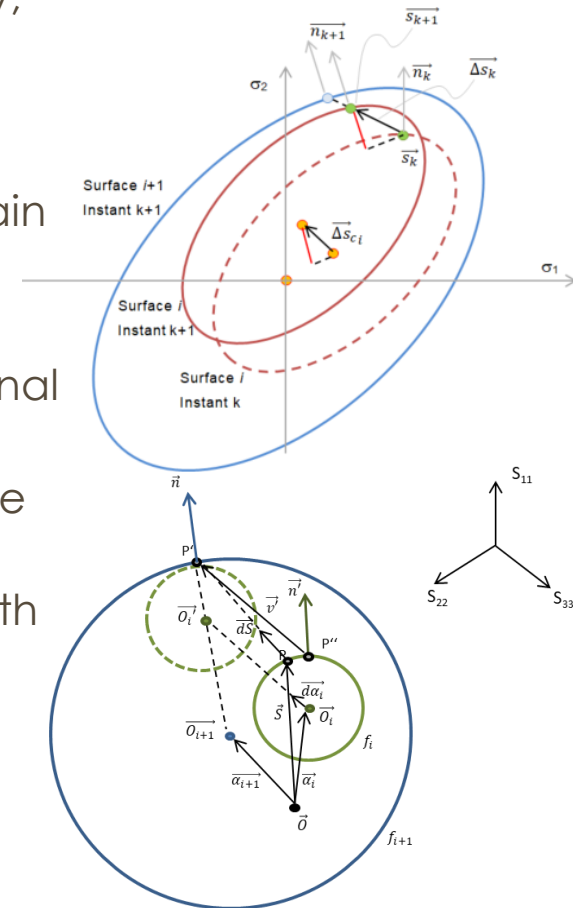
- Uniaxial reduction (\*) analysis based on S-N curves with Goodman, Gerber, Soderberg, Walker, Morrow, Smith-Watson-Topper, Haigh methods for mean stress levels accounting (it can also be decided not to consider mean stress corrections)
  - Uniaxial reduction (\*) analysis based on military standard S-N curves
  - Dang-Van, McDiarmid multiaxial stress based analysis
  - Reserve Factor calculation based on Goodman-Smith diagram
- 
- (\*) Uniaxial Reduction consists in a fatigue analysis carried out considering one stress contribution: the elemental stress tensor time history is projected at different angles and for each one the fatigue Life is calculated. The minimum Life is retained as element Life

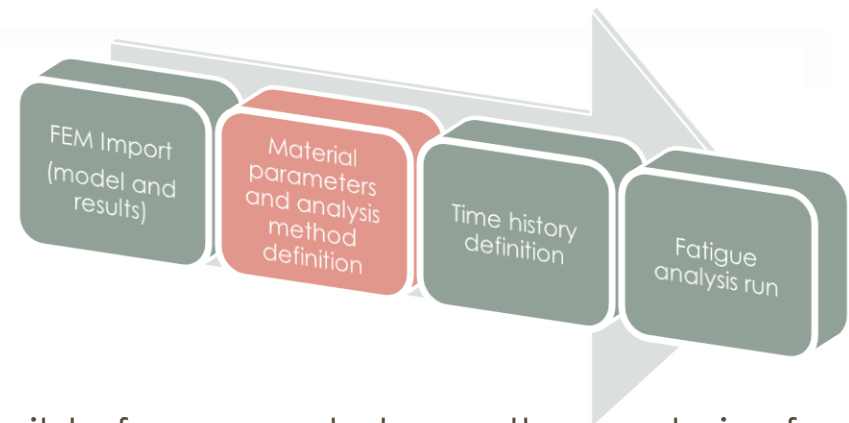
# LIFING.Life



- Strain based methods

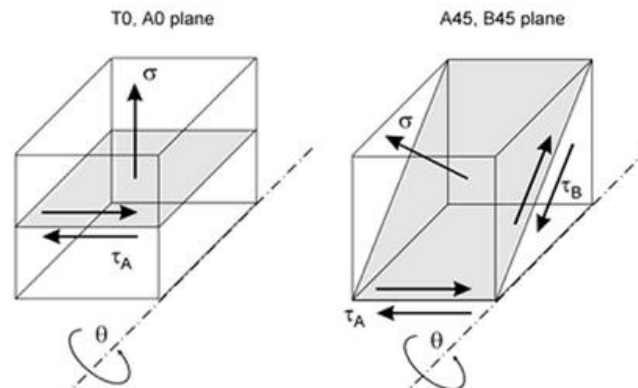
- Uniaxial reduction analysis based on e-N curves with Morrow, Smith-Watson-Topper, Manson-Halford methods for mean stress levels accounting (it can also be decided not to consider mean stress corrections)
  - Plastic stress-strains derived with Neuber or Equivalent Strain Energy Density (Glinka) methods
- Multiaxial strain based analysis can be performed with
  - **Hoffman-Seeger** or **Dowling** methods in case of Proportional Loading situations
  - Köttegen-Barkey-Socie **Pseudo-Material Approach** in case of Non-Proportional Loading situations
    - Elastic-Plastic stress/strain time histories are derived with the Mroz-Garud cyclic plasticity model





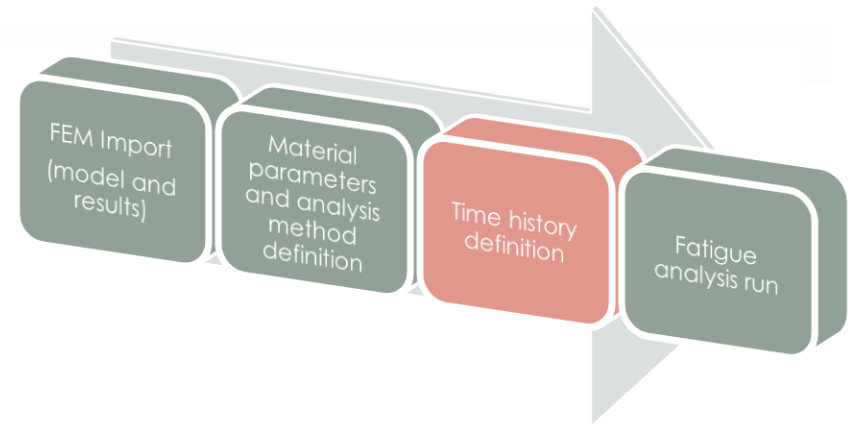
- Strain based methods

- The user decides which method to use (it is possible for example to run the analysis of Non-Proportional Loading cases with Hoffman-Seeger or Dowling methods: in this case 'average' principal angles and biaxiality ratios are calculated and the analysis is carried out considering the stress time history projected on this plane and accounting the calculated biaxiality ratio
- Implemented Fatigue parameters in case of Multiaxial Fatigue analysis:
  - Smith-Watson-Topper (plane T0)
  - Fatemi-Socie (planes A0, A45, B45)
  - Brown-Miller (with and without mean stress corrections) (planes A0, A45, B45)

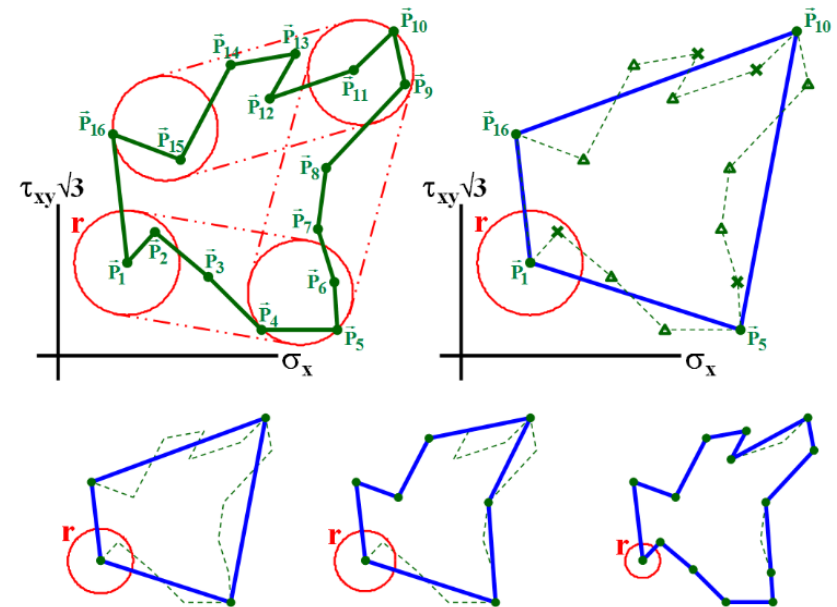




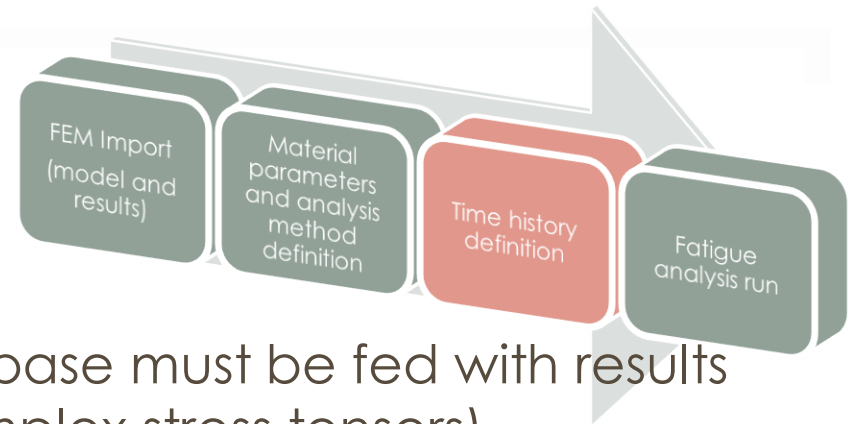
# LIFING.Life



- The time history is defined on the basis of the imported result load cases
  - One sequence can be defined for each Load Case or ...
  - ... It can be defined a sequence of Load Cases combination
- The assembled element tensor time history can be filtered with a Racetrack Filter (in case of full multiaxial fatigue analysis with Pseudo-Material a multiaxial Racetrack filter is used)

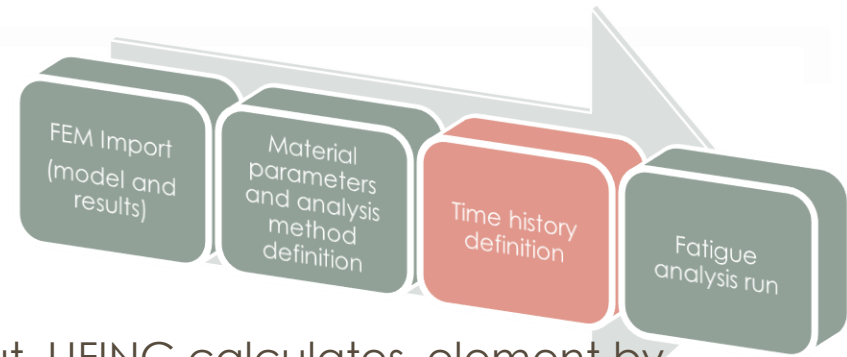


# LIFING.Life

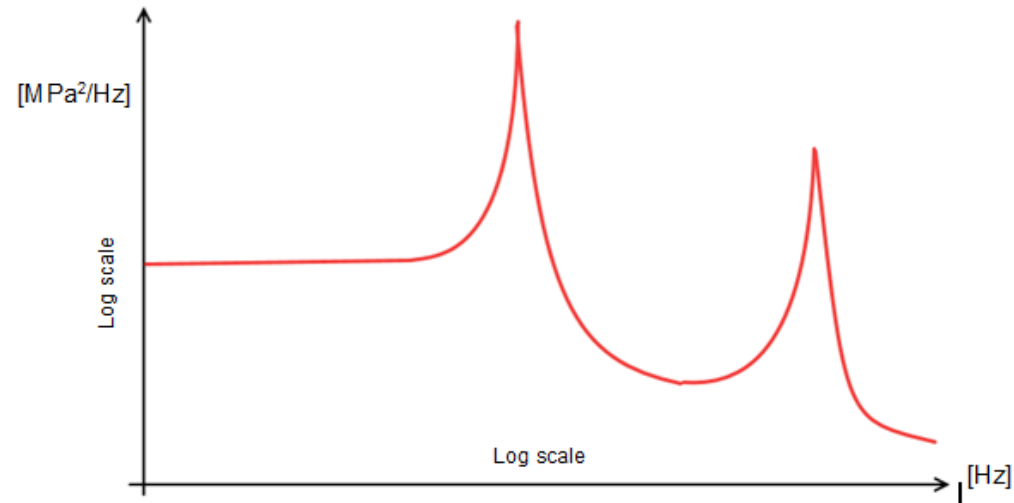


- If the analysis is based on PSD the database must be fed with results from Frequency Response analysis (complex stress tensors).
- LIFING calculates the corresponding Von Mises stress, from the complex tensor, for each frequency.
- An input PSD is provided, which acts as multiplier for the Frequency Response analysis results.
- Cycles are calculated with Dirlik, Narrow Band and Stainberg methods

# LIFING.Life

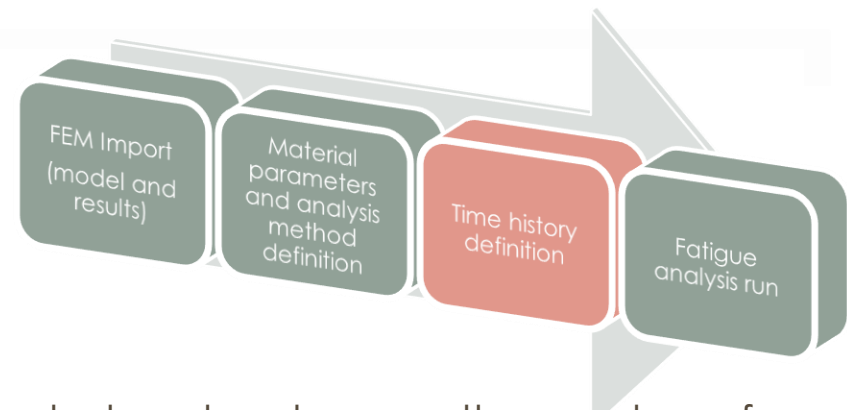


- From the FEM Frequency Response Analysis output, LIFING calculates, element-by-element, the Von Mises stress per g [MPa/g] (from the complex stress tensors).
- This quantity, to the power of 2, is scaled by the user defined accelerations PSD [ $\text{g}^2/\text{Hz}$ ] and the Von Mises PSD [ $\text{MPa}^2/\text{Hz}$ ] is derived.

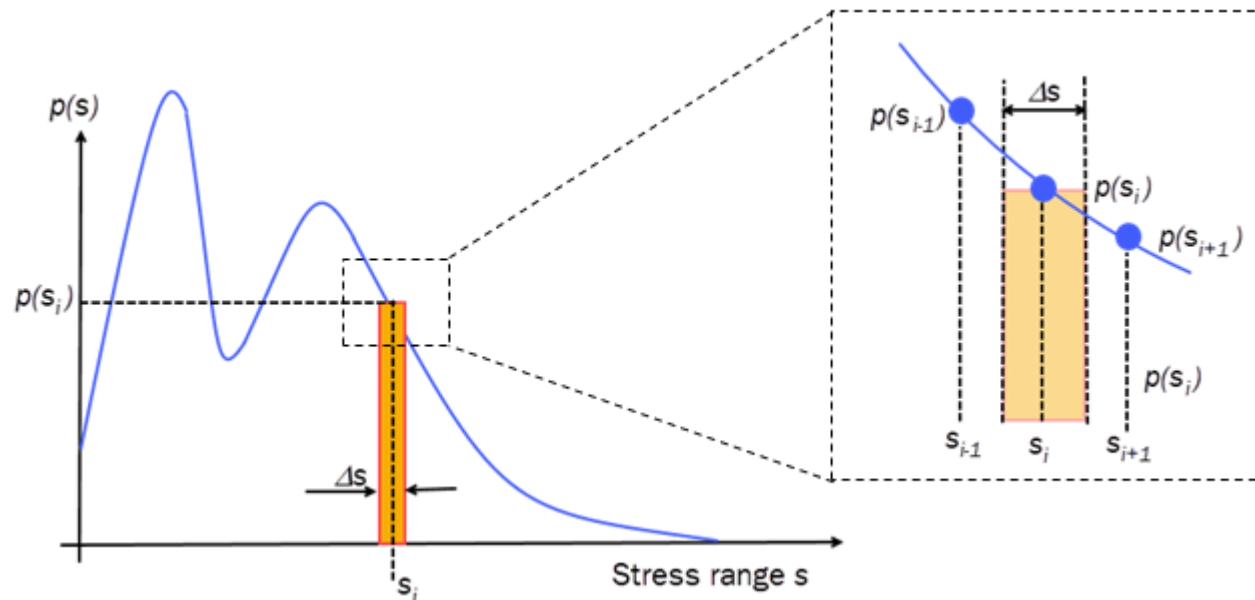


- The Dirlik or Narrow band can be therefore be applied to calculate the PDF (probability density function) of stress ranges  $s$ .

# LIFING.Life

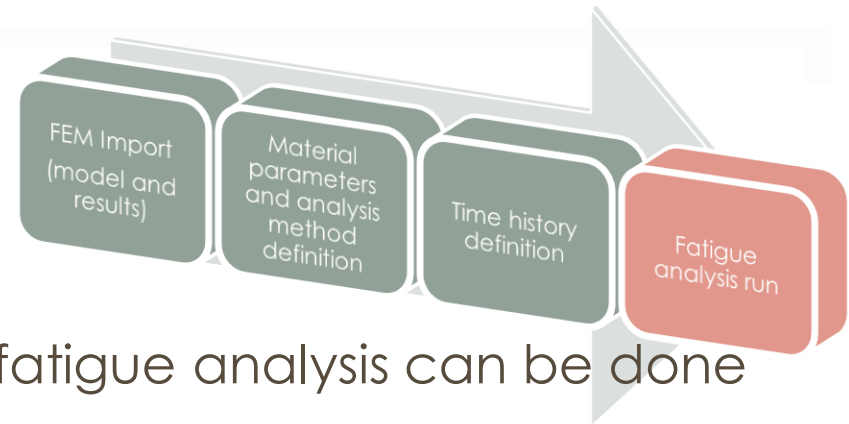


- The Dirlik method can be used to calculate, for each stress level range, the number of occurrences, to be used with stress or strain based methods and calculate fatigue Life.

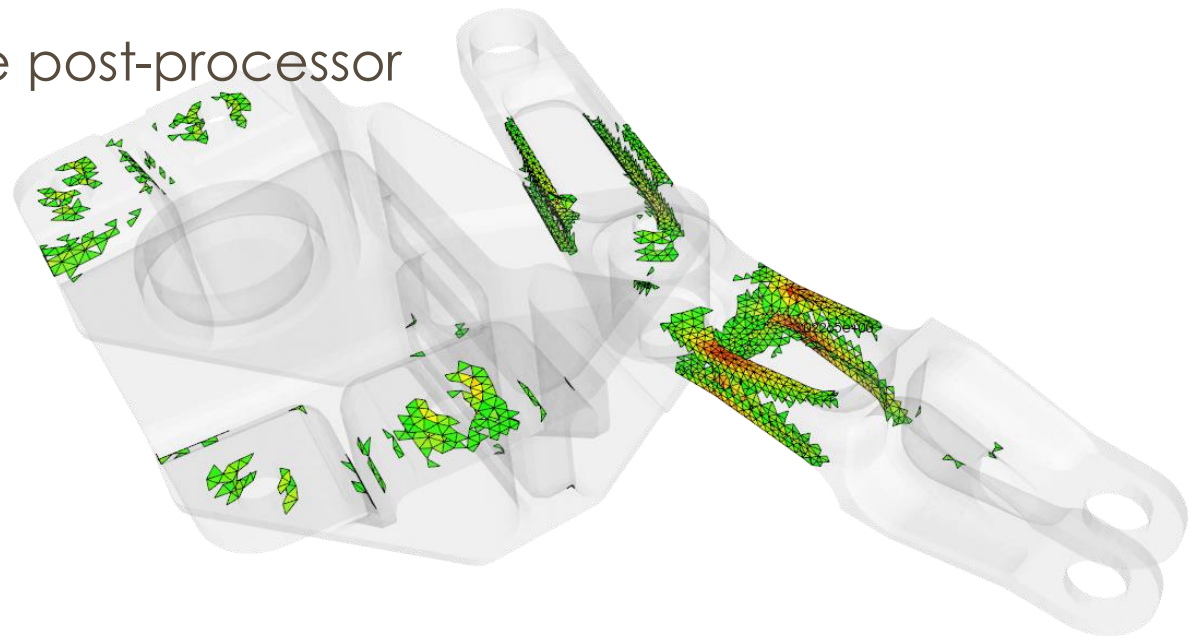


- Other methods such as Narrow Band and Stainberg can be used.

# LIFING.Life

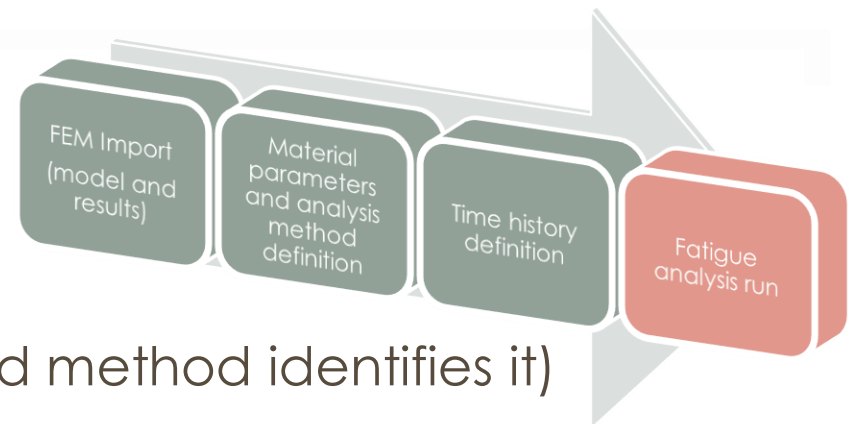


- Once the previous steps are done, the fatigue analysis can be done
  - On the entire FEM
  - On a defined set of Sub-Parts
  - On a defined Element
- Based on the defined analysis method, material properties, time history, etc.
- Fatigue Life is shown in the post-processor



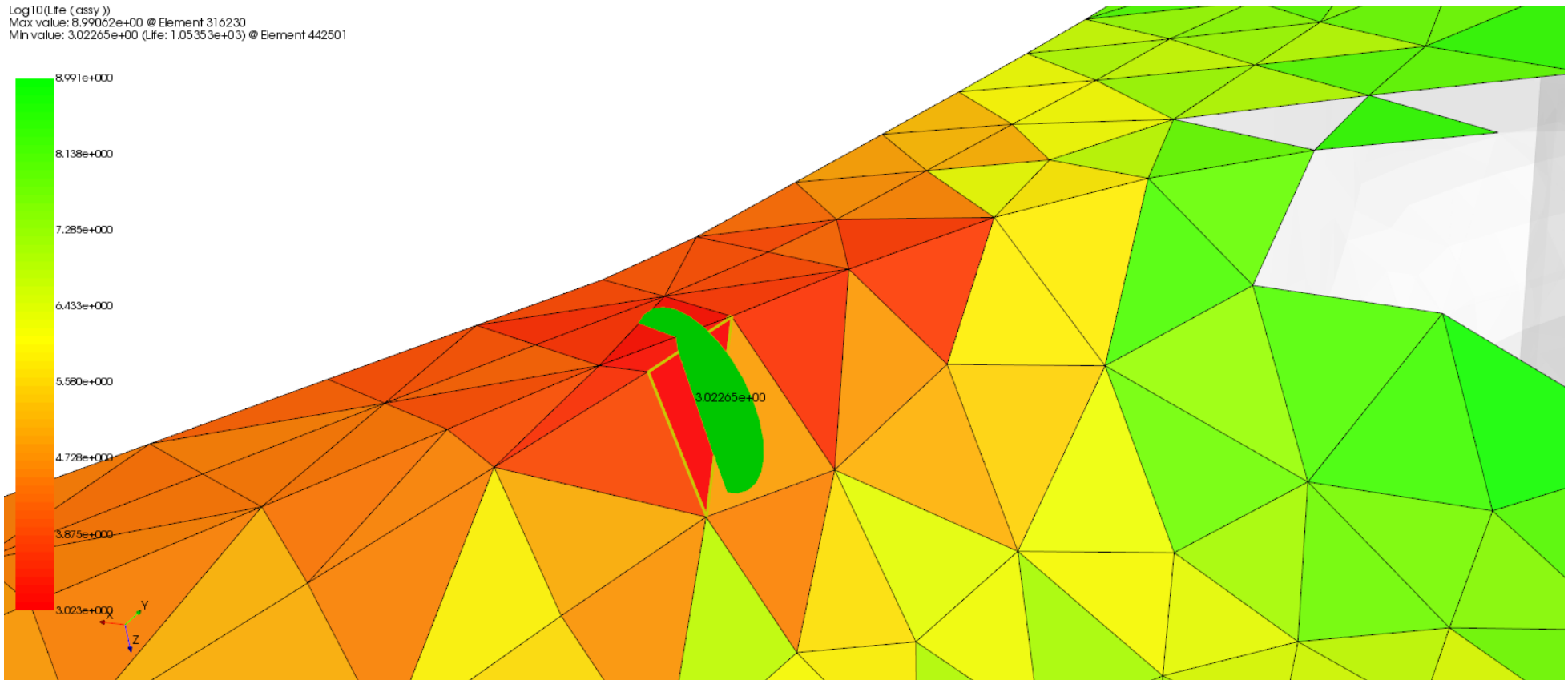


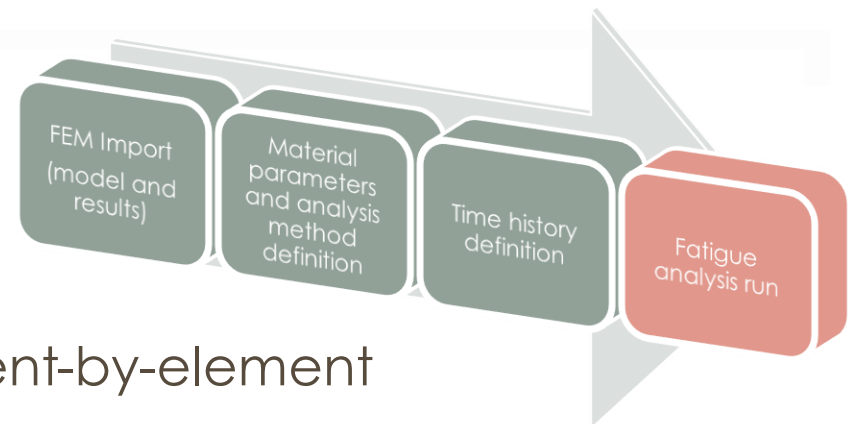
# LIFING.Life



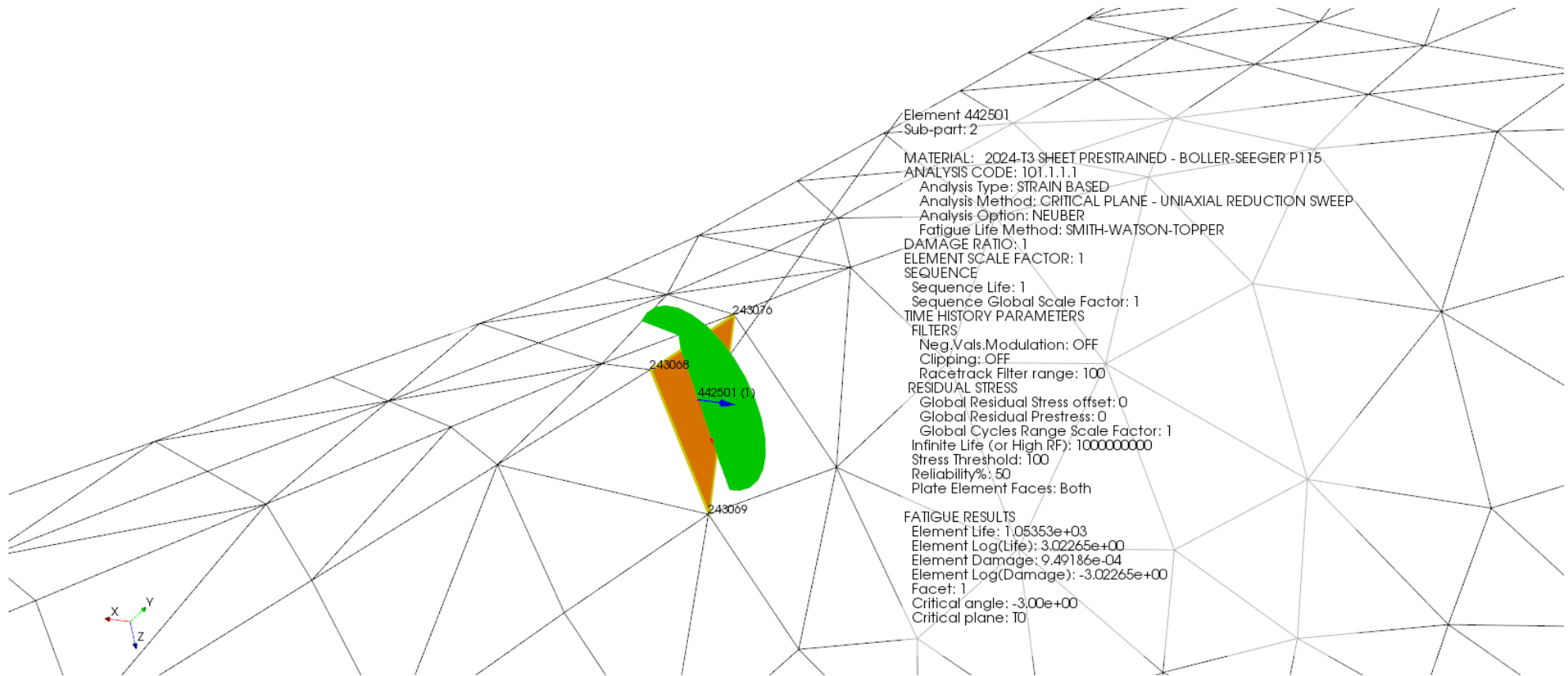
- The critical plane is shown (if the defined method identifies it)

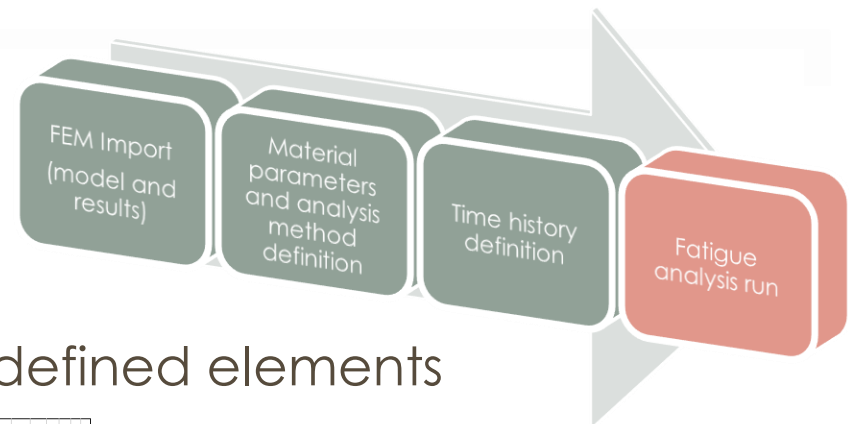
Log10(Life (assy))  
Max value: 8.99062e+00 @ Element 316230  
Min value: 3.02265e+00 (Life: 1.05353e+03) @ Element 442501



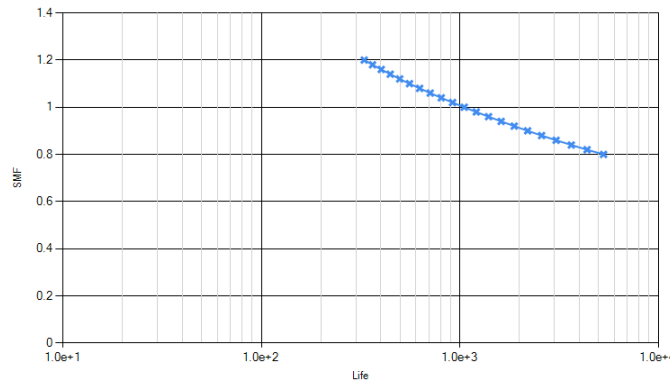


- The solution can be interrogated element-by-element





- The user can run 'sensitivity analysis' at defined elements



- LIFING provides in a ASCII file the breakdown of the damage calculation (useful for debugging the analysis or for further investigations)

Damage Calculation Breakdown

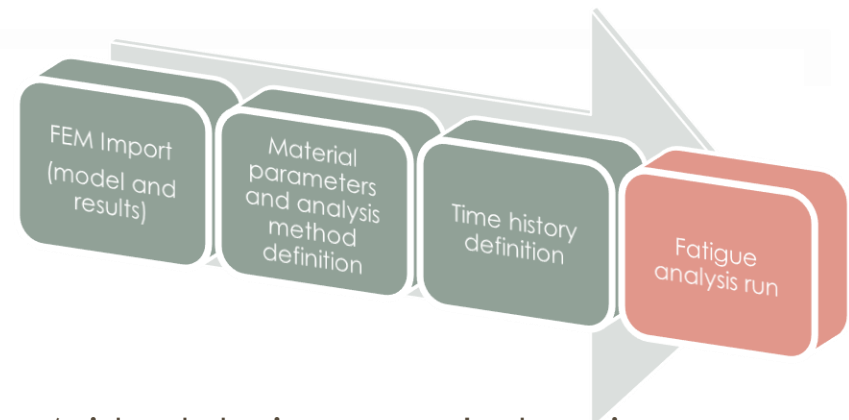
SMF: 1

Critical Plane Angle: -3.00000e+00

S_Max	S_Min	!d_S!	!d_sigma!	sigma_Max	eps_Max	!d_eps!	!d_eps_eq!	Ncycles	Occurrences	Part. damage	Cum. damage
303.42325	-390.59899	694.02224	693.89420	311.86615	3.958e-03	9.317e-03	4.416e-03	1.427e+04	1	7.006e-05	7.006e-05
312.56065	-395.43145	707.99210	707.78199	318.80406	4.11e-03	9.506e-03	4.51e-03	1.209e+04	1	8.271e-05	1.528e-04
249.91932	-346.42997	596.34929	596.34639	258.10593	3.243e-03	8.005e-03	3.724e-03	5.833e+04	1	1.714e-05	1.699e-04
364.88808	-425.44311	790.33119	787.32429	370.13271	4.826e-03	1.065e-02	5.143e-03	4.543e+03	1	2.201e-04	3.9e-04
448.27794	-433.26981	881.54774	856.88763	432.62125	6.235e-03	1.217e-02	5.945e-03	1.788e+03	1	5.592e-04	9.492e-04

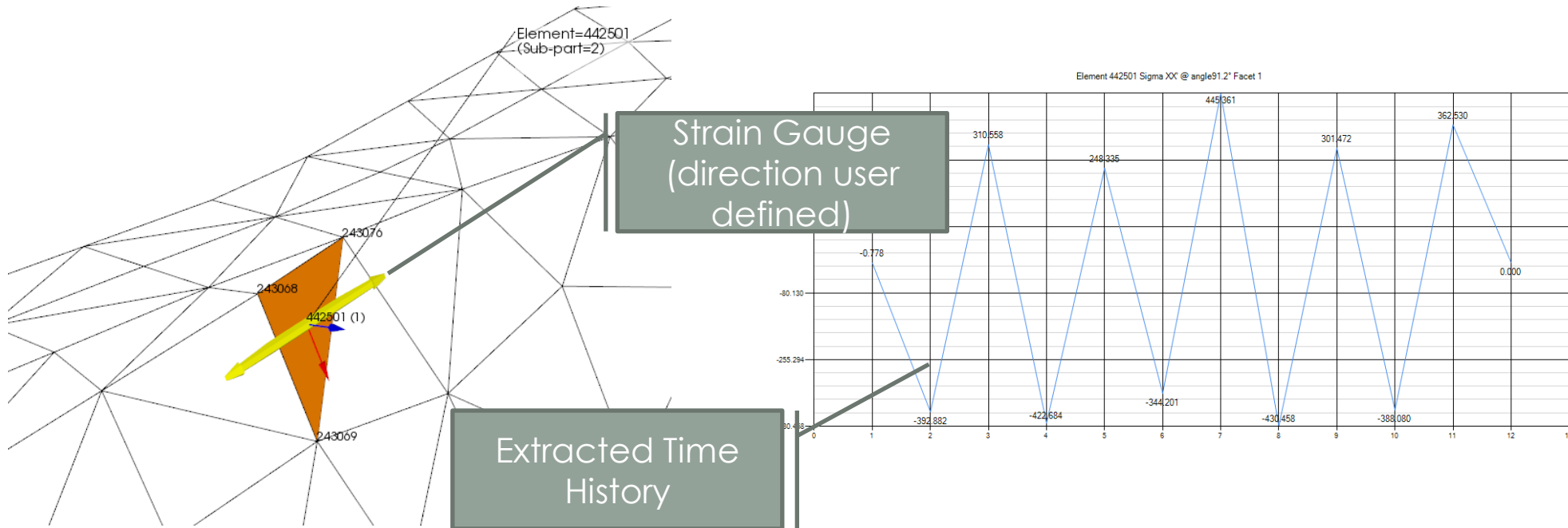
```

Life = 1.0535e+03
Life*D = 1.0535e+03
N = 1.0535e+03
N*LifeSeq = 1.0535e+03
Life = N*LifeSeq*D = 1.0535e+03
  
```

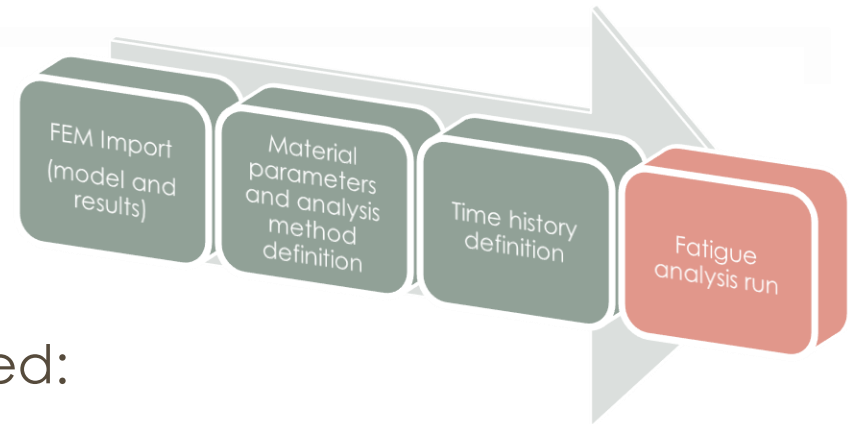


- VIRTUAL STRAIN GAUGE

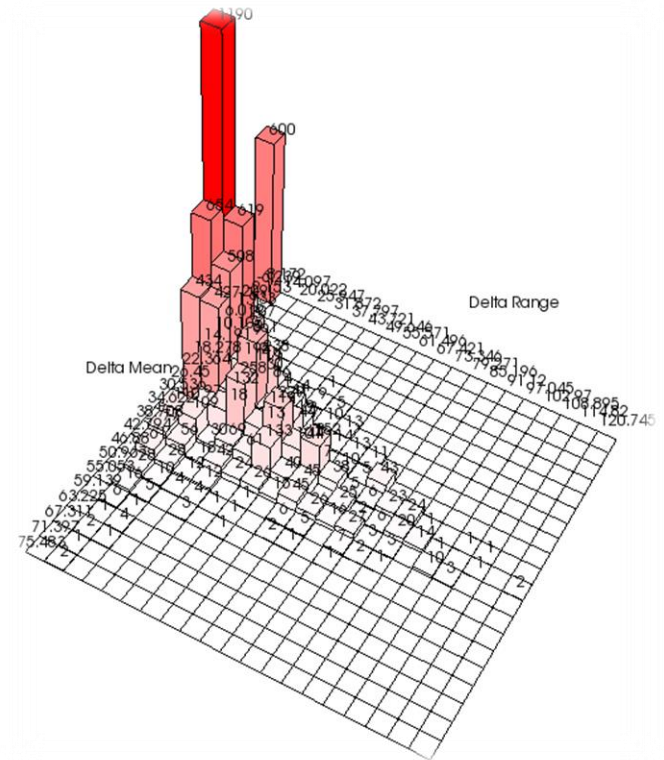
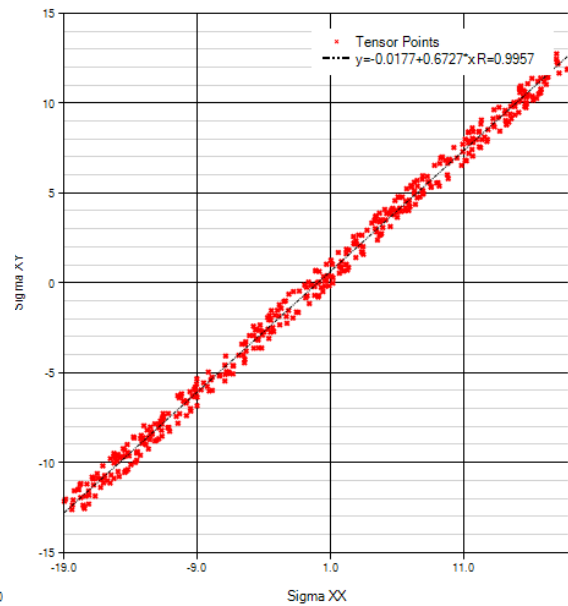
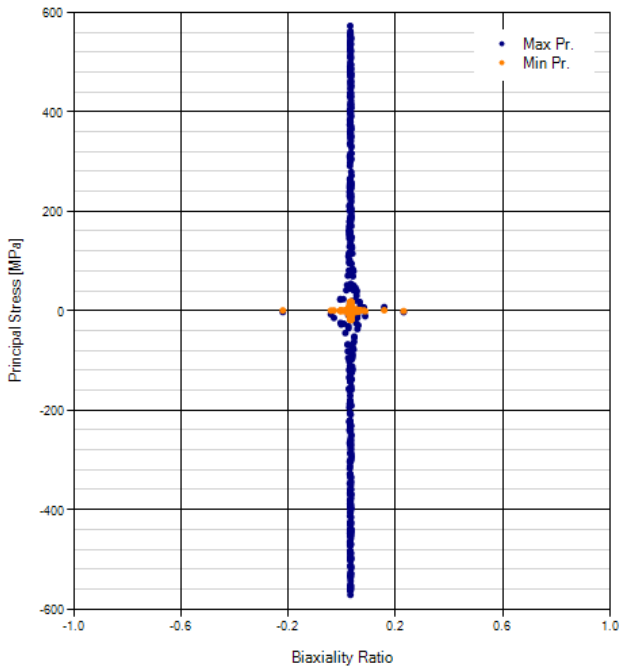
- The user can interrogate the model by putting a 'virtual strain gauge' at a given element, orient it at a given angle, and the related stress time history can be directly extracted



# LIFING.Life



- Additionally the following can be derived:
  - Biaxiality plots and histograms
  - Time histories cycle counting/filtering, ...

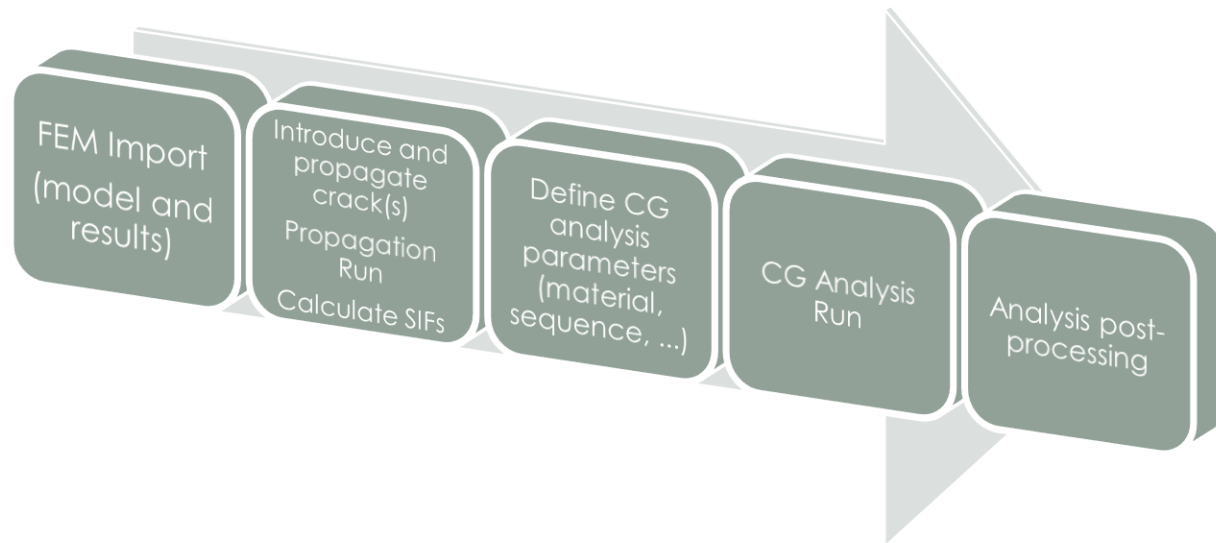


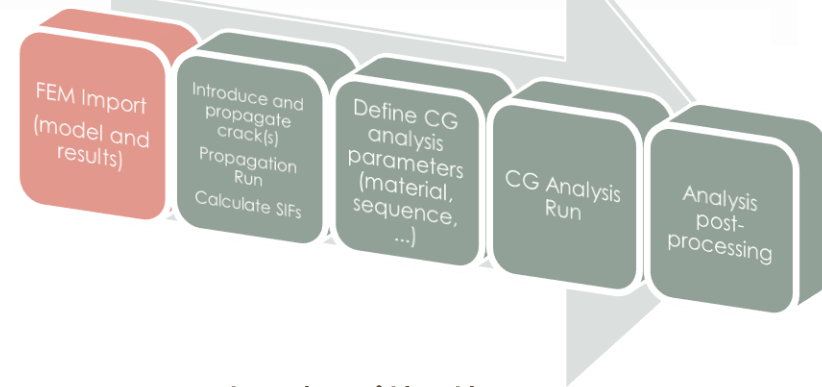


# LIFING.Growth

- LIFING has the capability to calculate crack growth in a FEM model
- Crack Growth in 2D (planar) or 3D geometries or Section Cuts of 3D meshes is solved.

The workflow:

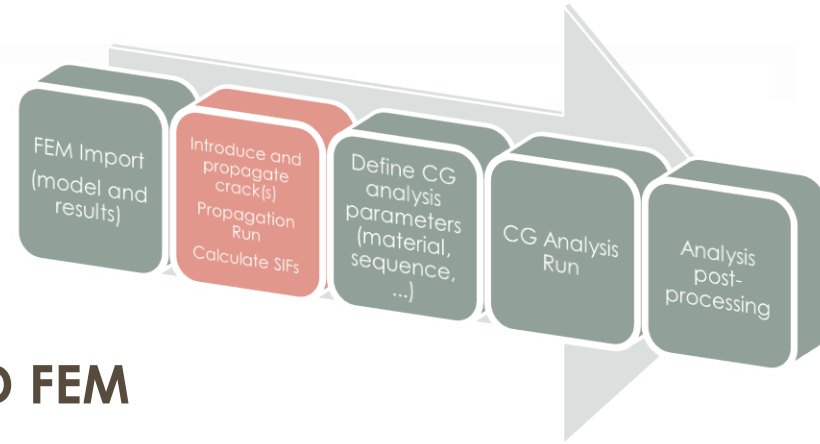




- **FEM Import**

- A FEM can be imported or internally generated with the QUICK2DFEM module.
- Depending on the FEM type, LIFING.GROWTH will calculate Stress Intensity Factors with J-Integral (2D) or M-Integral (3D) with the internally coded 2D and 3D solvers.
- In both cases the FEM is created such to have 2nd order elements with special templates at the crack tip (2D) or crack front (3D).

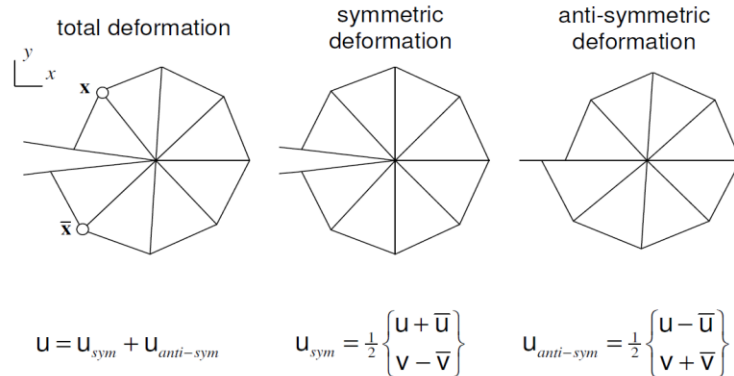
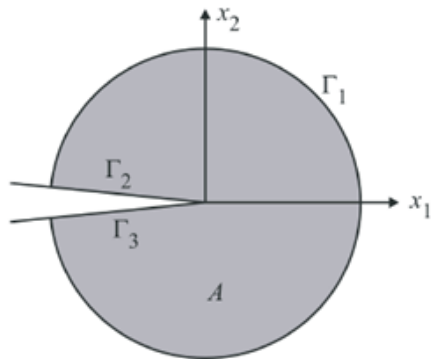
# LIFING.Growth



- **Crack(s) propagation simulation in 2D FEM**

- One or more cracks are introduced
- The FEM is remeshed, based on the crack propagation
- At the crack(s) tip, Stress Intensity Factors are calculated with J-Integral method (using quarter point elements)

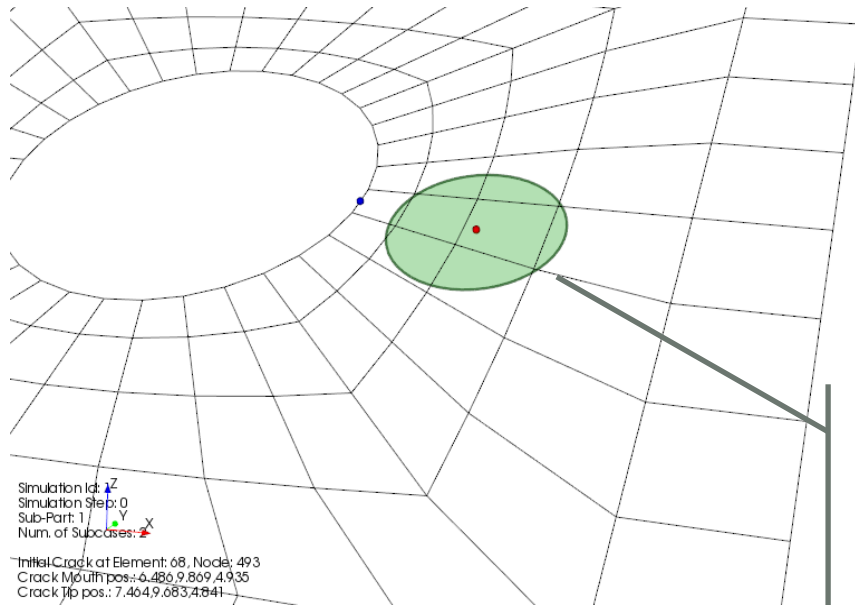
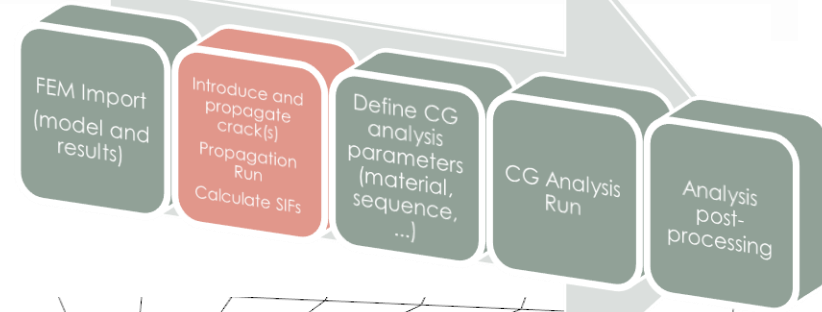
$$J = \int_{\Gamma} \left( W n_x - T_i \frac{\partial u_i}{\partial x} \right) ds \rightarrow \bar{J} = \int_A \left[ \sigma_{ij} \frac{\partial u_i}{\partial x_1} - W \delta_{1j} \right] \frac{\partial q_1}{\partial x_j} dA \rightarrow J = G = \frac{1 - \nu^2}{E} (K_I^2 + K_{II}^2)$$



$$G_I = J_I = J(u_{sym}, \sigma_{sym})$$

$$G_{II} = J_{II} = J(u_{anti-sym}, \sigma_{anti-sym})$$

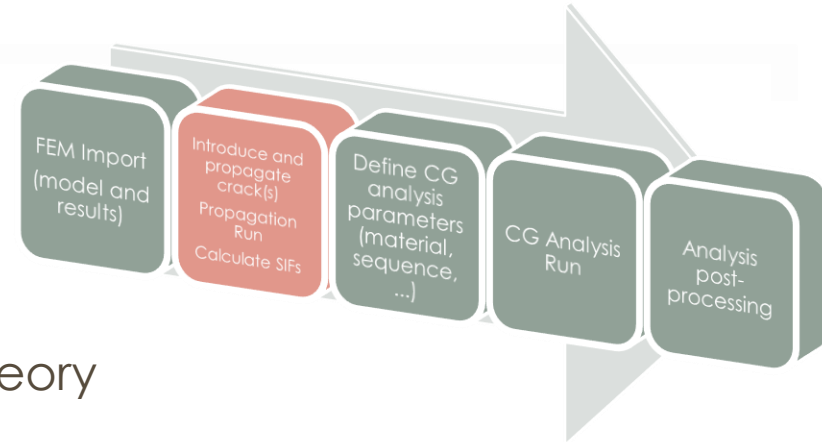
# LIFING.Growth



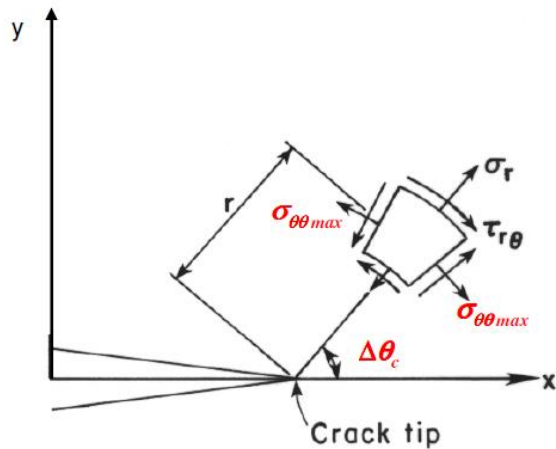
Initial Crack Definition  
The analyst decides the orientation, length and level of refinement

- After being introduced, the crack(s) propagation is performed automatically

# LIFING.Growth

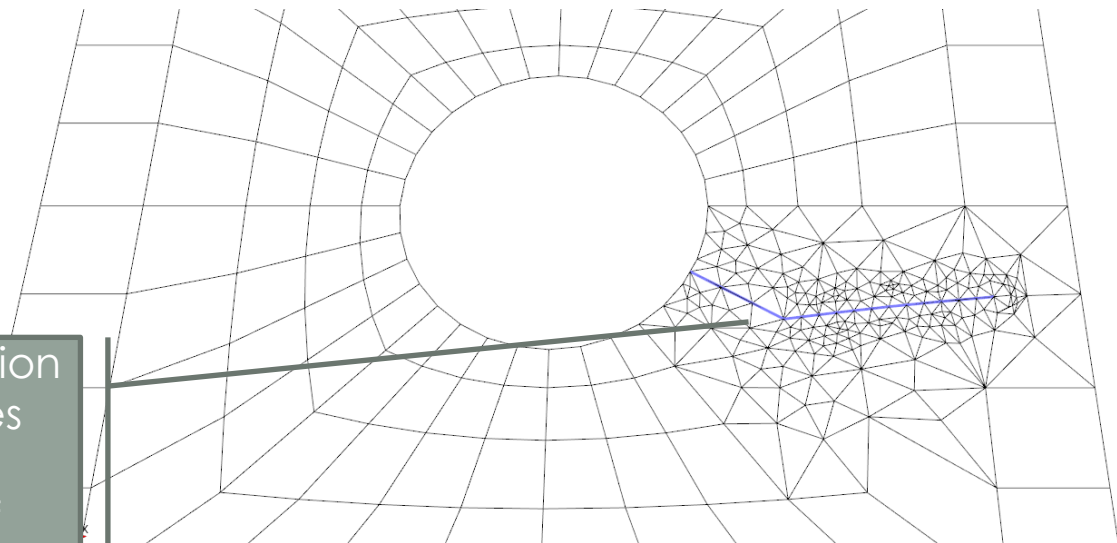


- Crack Kinking calculated with the  $\sigma_{\theta\theta,max}$  theory



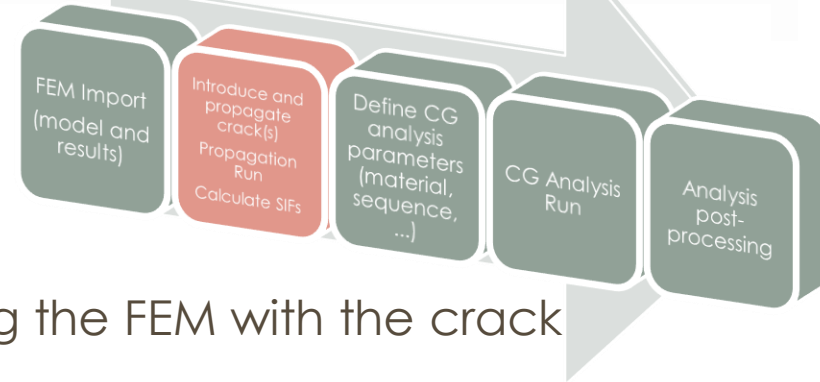
$$\frac{K_{II}}{K_I} = \frac{-\sin \Delta\theta_c}{(3\cos \Delta\theta_c - 1)} \quad \rightarrow \quad \Delta\theta_c = 2 \tan^{-1} \left( \frac{1 - \sqrt{1 + 8(K_{II}/K_I)^2}}{4(K_{II}/K_I)} \right)$$

Initial Crack Definition  
The analyst decides the orientation, length and level of refinement

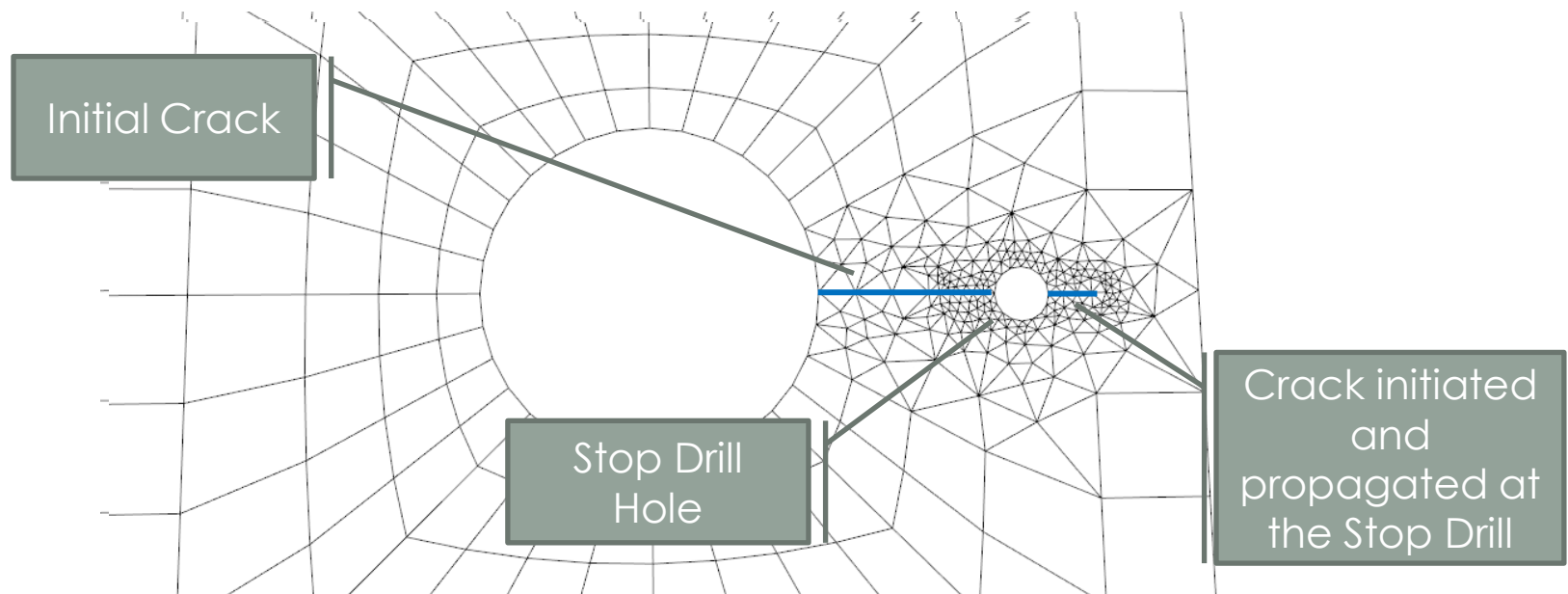




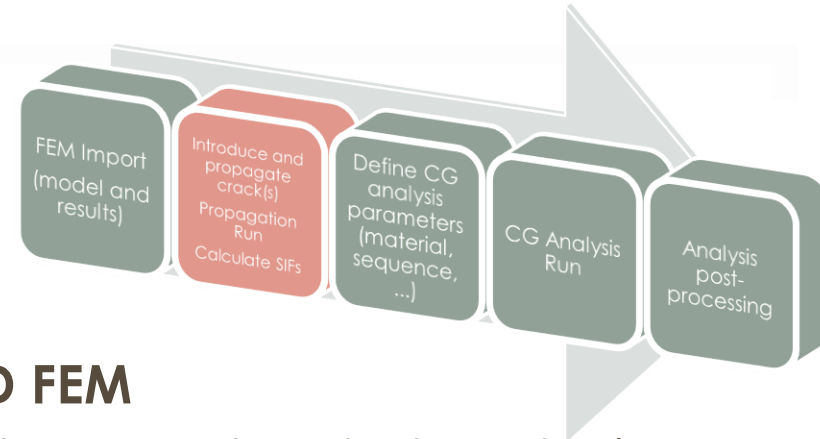
# LIFING.Growth



- An internal mesher is in charge of rebuilding the FEM with the crack discontinuities
- An internal solver is in charge of calculating stress and deformations at each crack propagation step
- Not only cracks can be introduced, but also holes to stop drill cracks



# LIFING.Growth

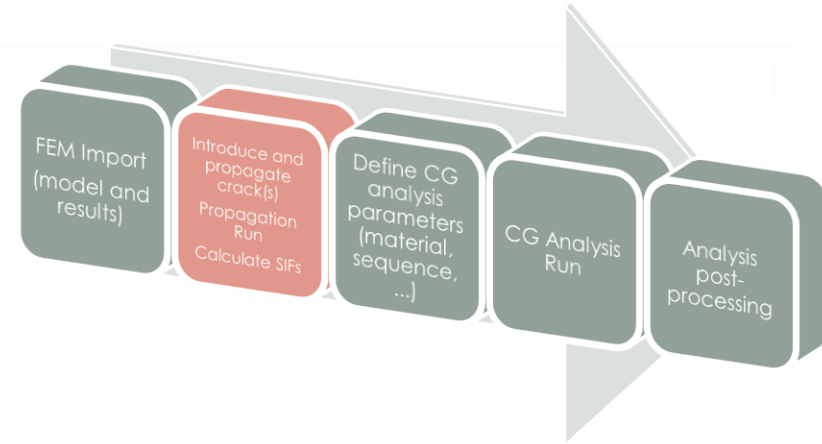


- **Crack(s) propagation simulation in 3D FEM**

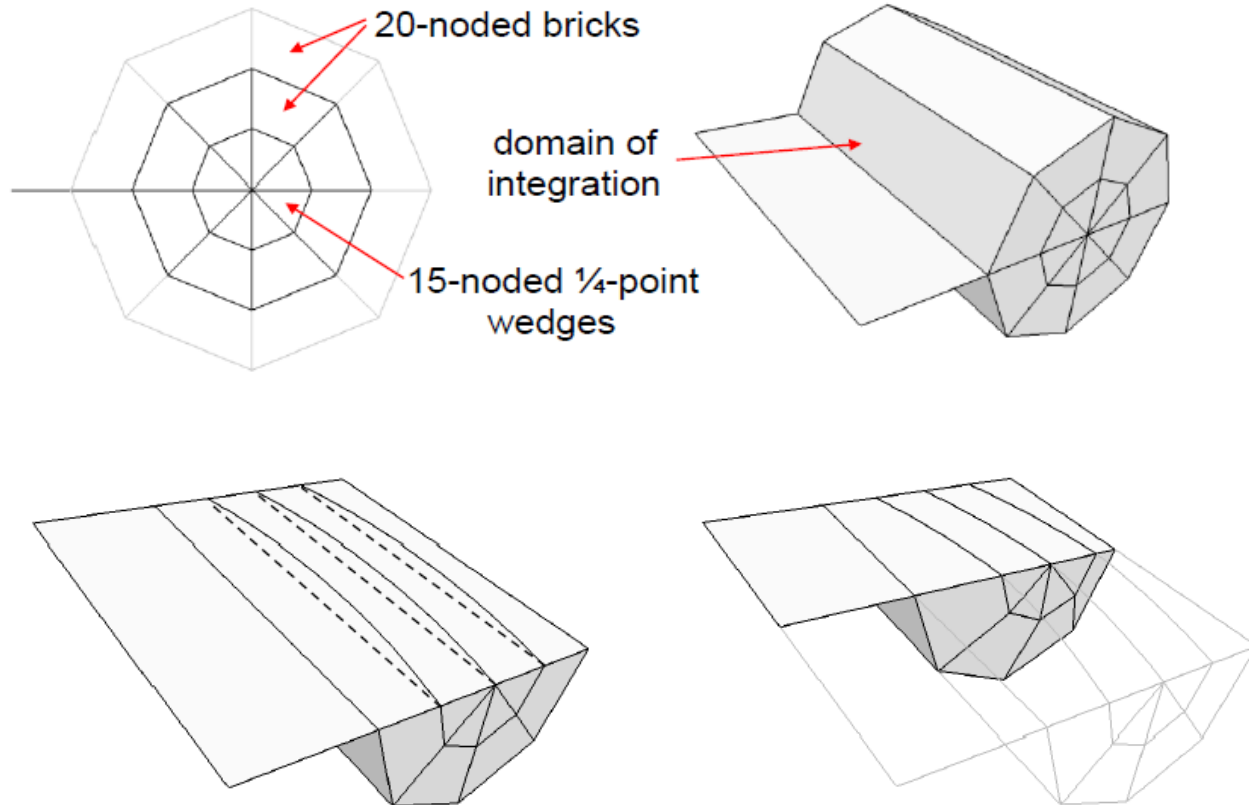
- The module Quick2DFEM can be used to generate a 3D by extrusion of a 2D mesh which is simply generated with the QUICK2DFEM script.
- Both linear and circumferential extrusions are allowed.
- A special QUICK2DFEM card is used to introduce a crack front (elliptic or parabolic or linear shape).
- Once generated, the FEM with the crack front is solved and Stress Intensity Factors are calculated with M-Integral

$$M^{(1,2)} = \int_{\Gamma} \left( \sigma_{ij}^{(1)} \frac{\partial u_i^{(2)}}{\partial x_1} + \sigma_{ij}^{(2)} \frac{\partial u_i^{(1)}}{\partial x_1} - W^{(1,2)} \delta_{1j} \right) \frac{\partial q}{\partial x_j} ds =$$
$$= \frac{1 - \nu^2}{E} K_I^{(1)} K_I^{(2)} + \frac{1 - \nu^2}{E} K_{II}^{(1)} K_{II}^{(2)} + \frac{1 + \nu^2}{E} K_{III}^{(1)} K_{III}^{(2)}$$

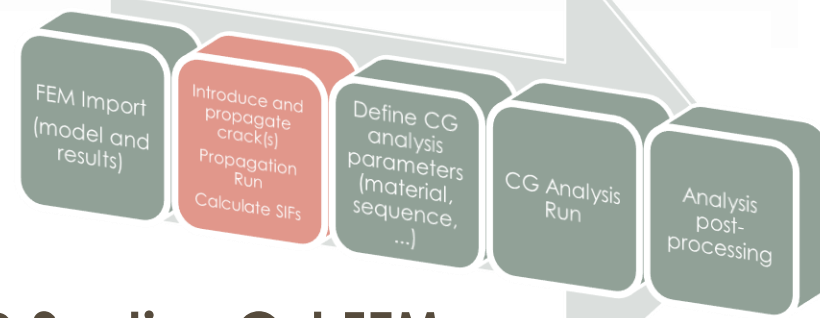
# LIFING.Growth



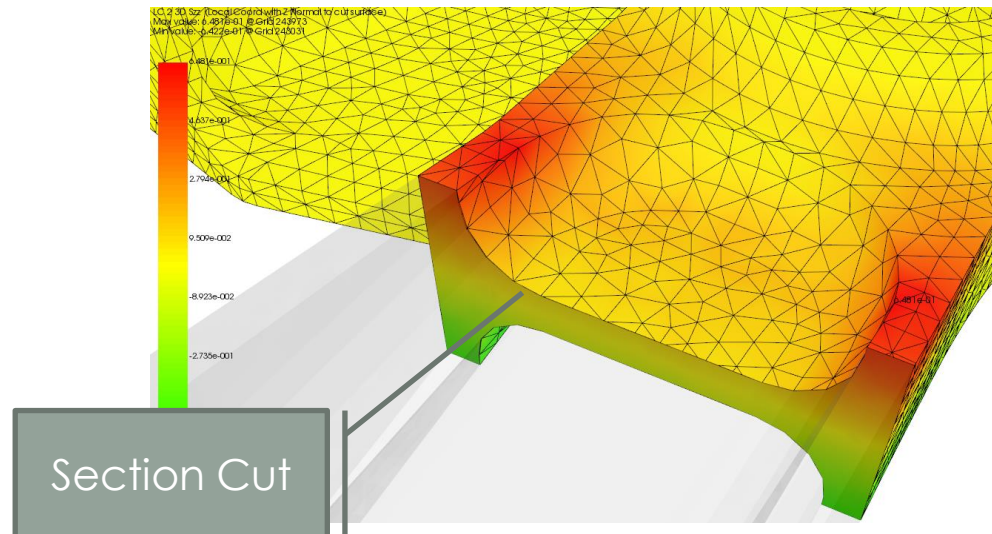
- A special template of elements are used



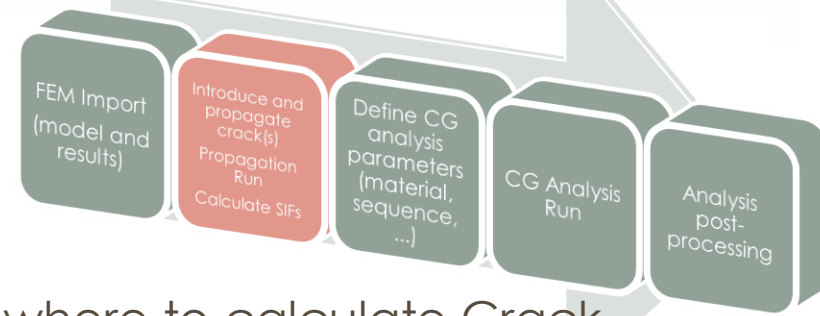
# LIFING.Growth



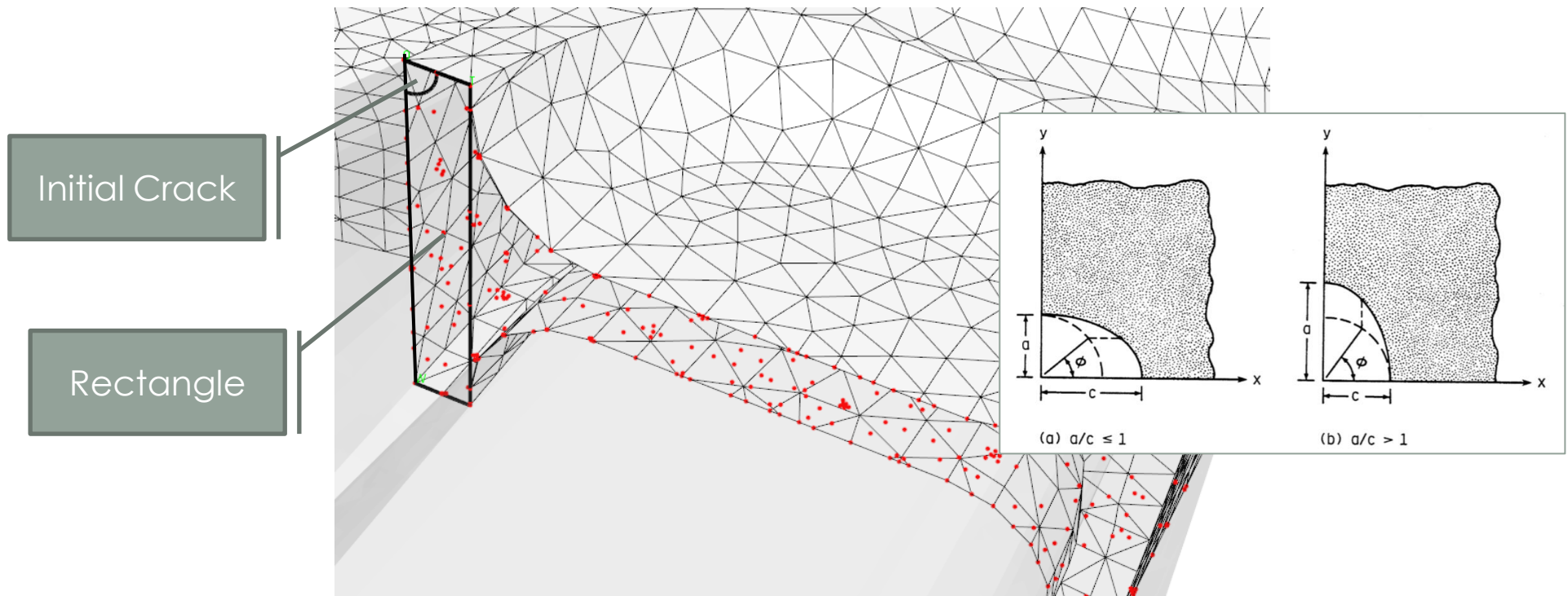
- **Crack(s) propagation simulation in 3D Section Cut FEM**
  - Lifing offers the possibility to perform quick Crack Growth estimation at section cuts
  - Nodal stress results must be preliminarily imported, in order to have stress data «inside» the FEM
  - A Section Cut is defined by the user (or automatically at the location showing minimum Crack Initiation Life)



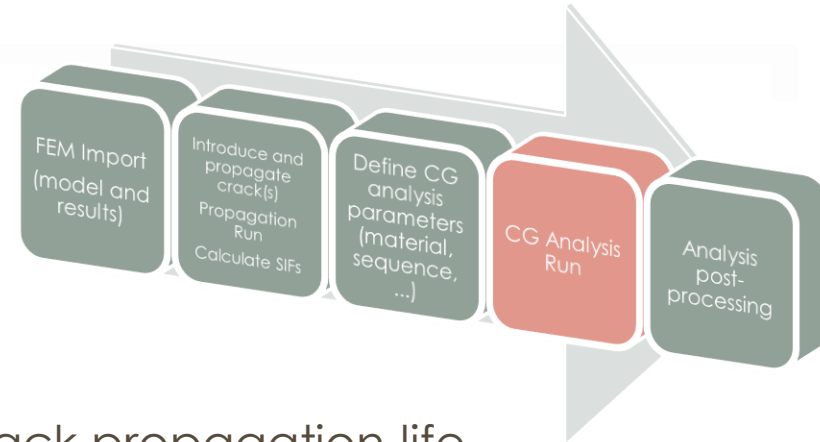
# LIFING.Growth



- The user defines a Rectangular portion where to calculate Crack Growth (engineering approach using Newman-Raju corrected with Glinka's Weight Functions)
- An initial crack (corner or pass-through) is defined



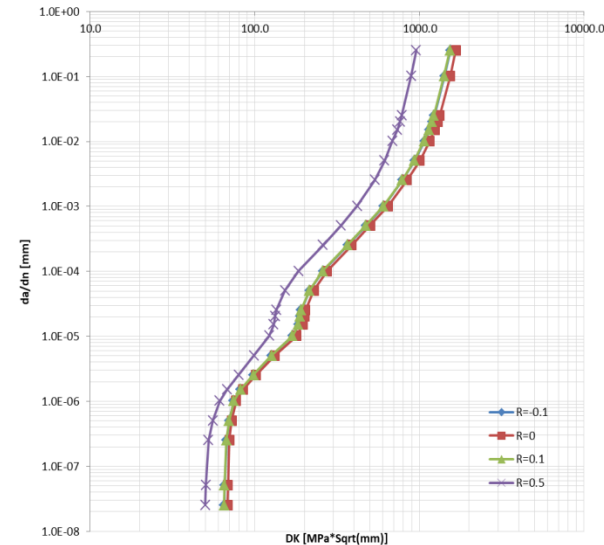
# LIFING.Growth



- **Crack Growth calculation**

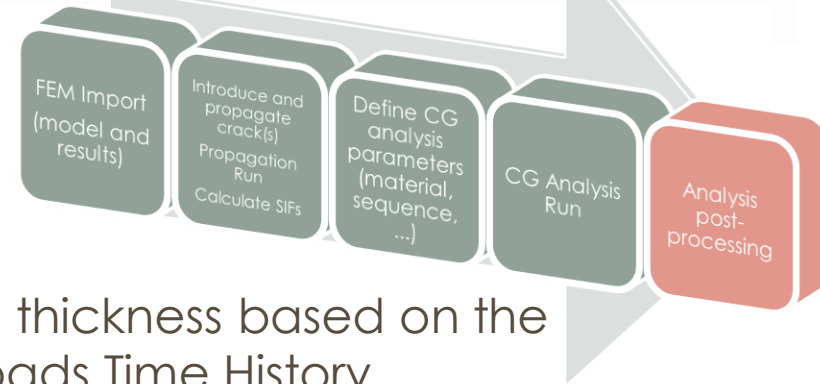
- NASGRO model is used to calculate crack propagation life

$$\frac{da}{dN} = C \left[ \left( \frac{1-f}{1-R} \right) \Delta K \right]^n \frac{\left( 1 - \frac{\Delta K_{th}}{\Delta K} \right)^p}{\left( 1 - \frac{K_{max}}{K_{crit}} \right)^q}$$

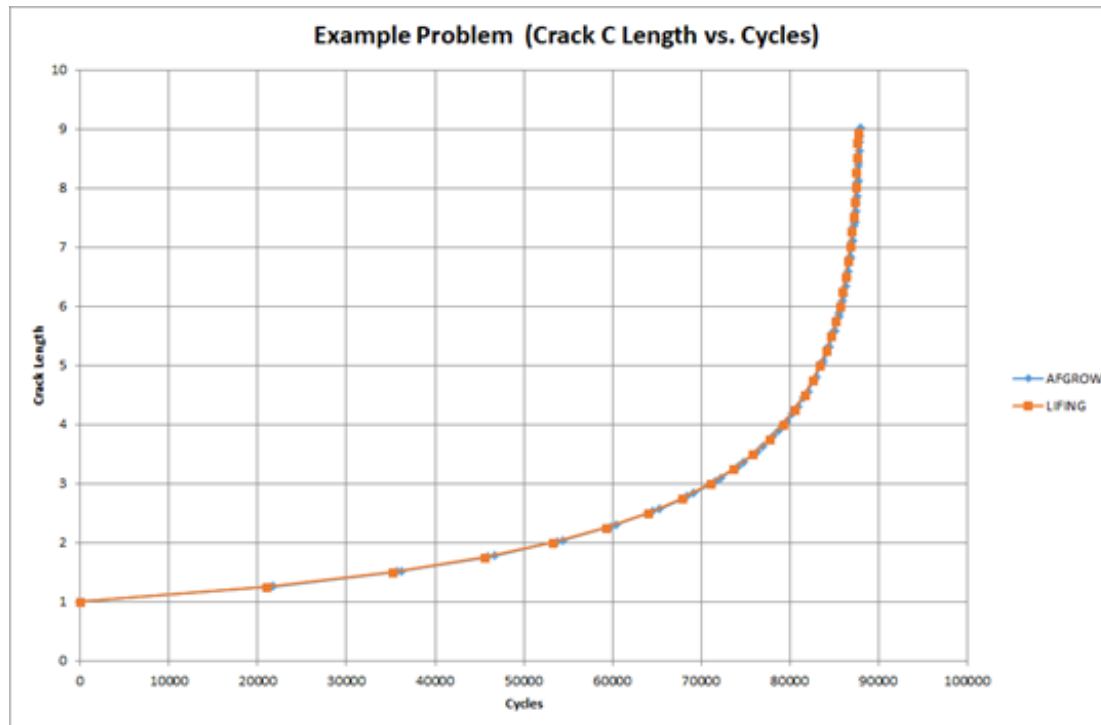


- Alternatively da/dN in tabular format can be used
- Multiple cracks growth calculated (relative growth rate accounted with Paris law)
- Generalized Willemborg Crack Closure model implemented

# LIFING.Growth

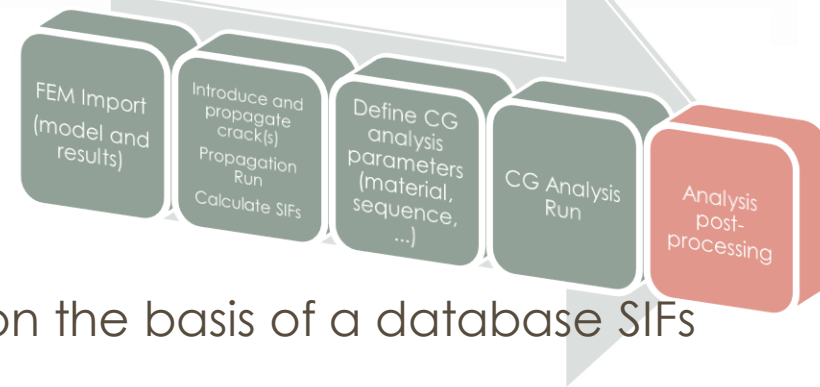


- The crack is automatically grown in the thickness based on the material NASGRO data and applied Loads Time History
- Implemented approach provides excellent adherence to AFGROW solution

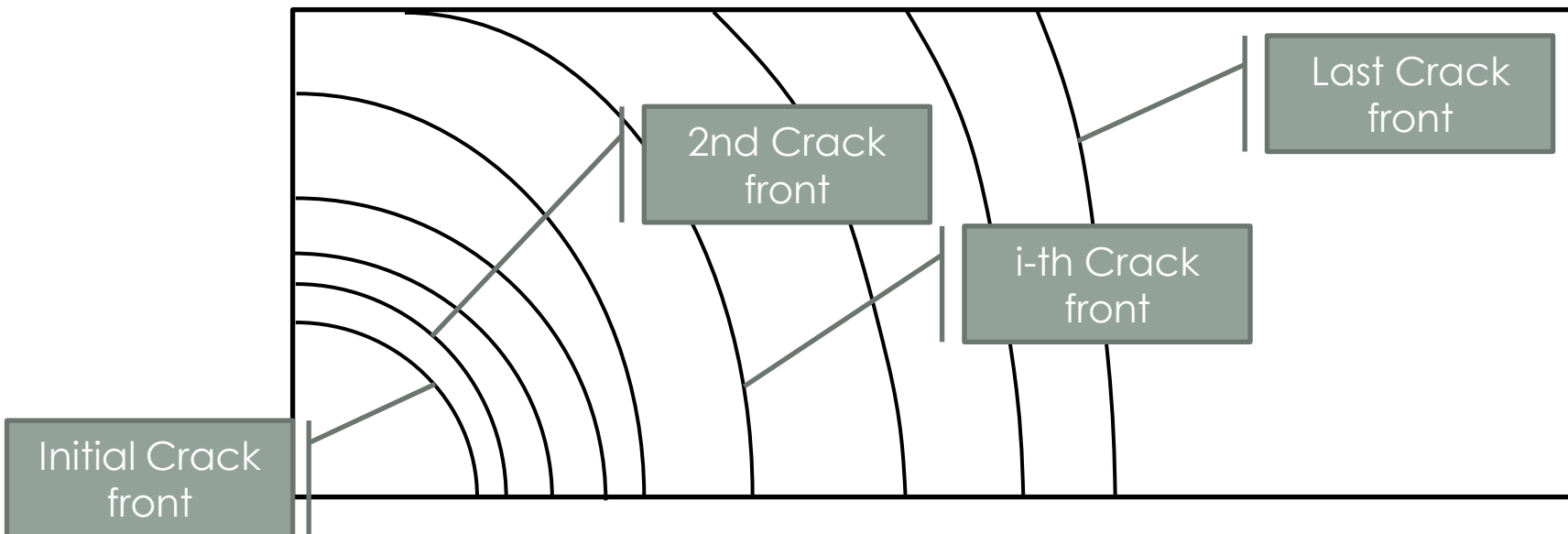




# LIFING.Growth



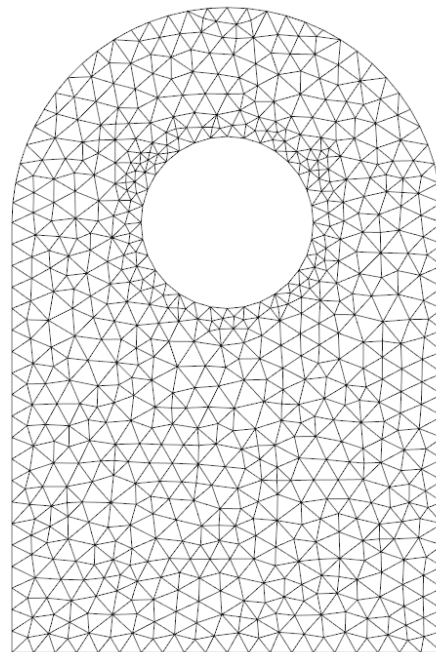
- A CG analysis can also be performed on the basis of a database SIFs externally calculated (from other SW)
- LIFING in this case uses the crack front computed SIFs and uses a 2D interpolator to evaluate correct SIFs while the crack is propagating



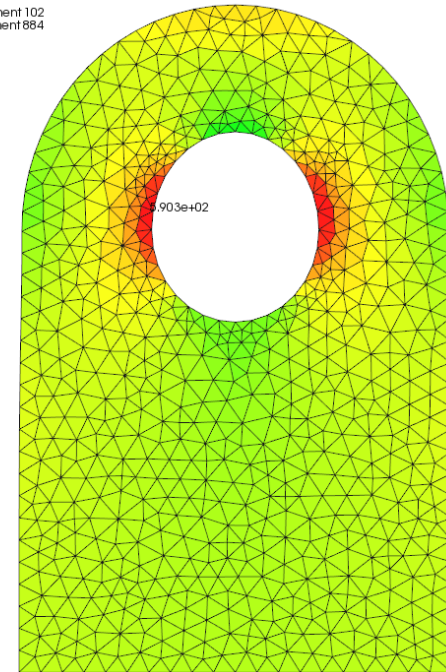
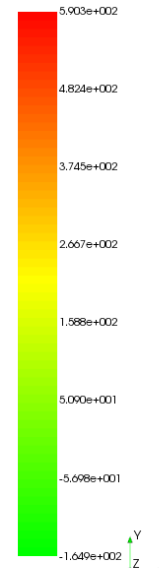
# QUICK2DFEM

- QUICK2DFEM provides the capability to run fatigue analyses on 2D and 3D FEM generated with simple script files
- The user defines model edges (straight or curved) with number of elements, holes, boundary conditions and material properties, in a simple file format
- The 2D model is immediately built and solved with the internal 2D solver

```
thick 1
smode 0
material 70000 .33
point 1 0 0
point 2 10 0
point 3 10 10
point 4 0 10
point 5 5 15
point 6 5 0
edge 1 0 1 6 10
edge 2 0 6 2 10
edge 3 0 2 3 20
edge 4 1 3 4 5 34
edge 5 0 4 1 20
hole 1 5 10 2 32
dedge 1 1 2 0
dedge 1 2 2 0
dpoint 1 1 12 0
fhole 1 1 1000 90 180
dump spc gpf
```

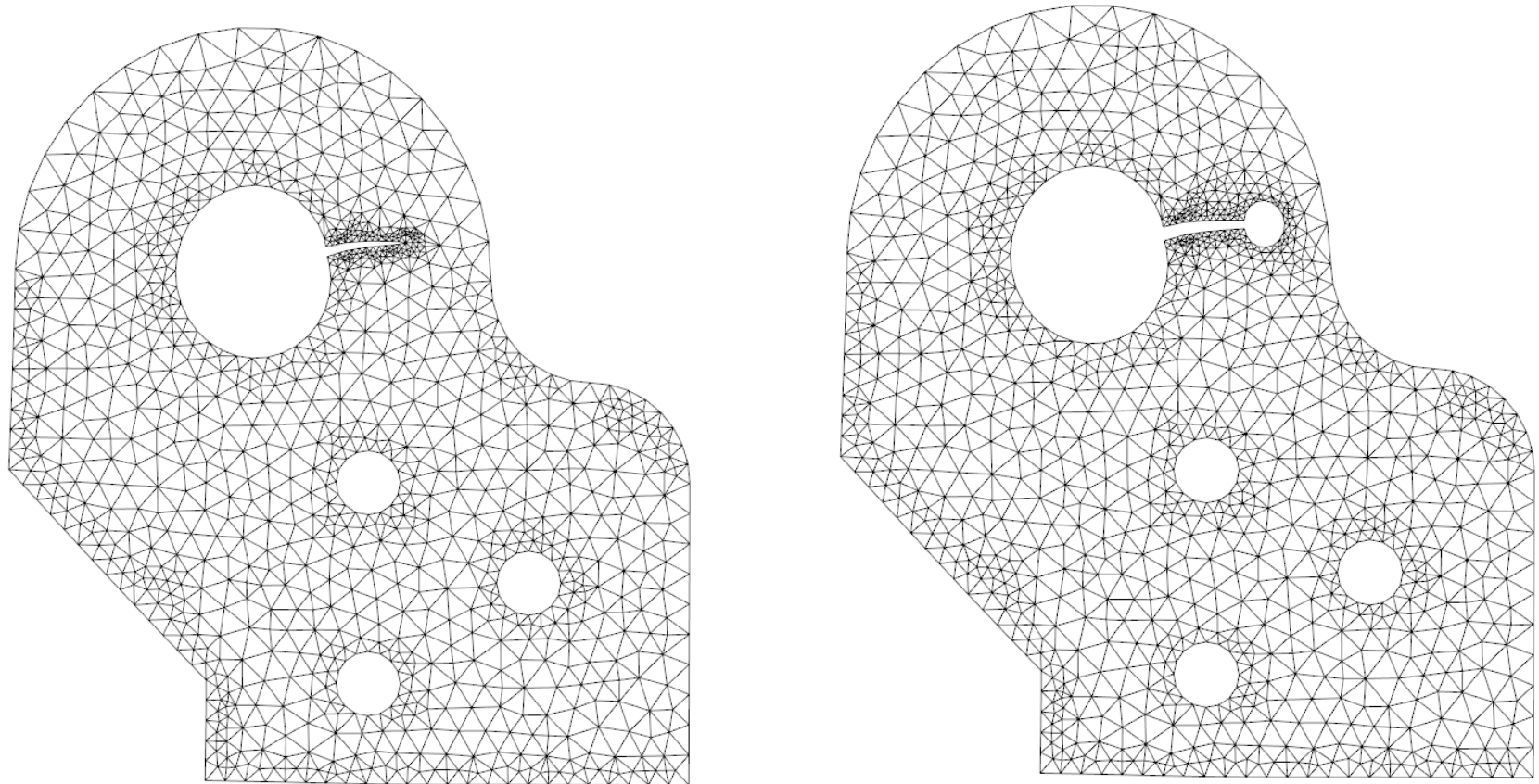


LC 1 Elm2D, Smax+  
Max value: 5.903e+02 @ Element 102  
Min value: -1.649e+02 @ Element 884



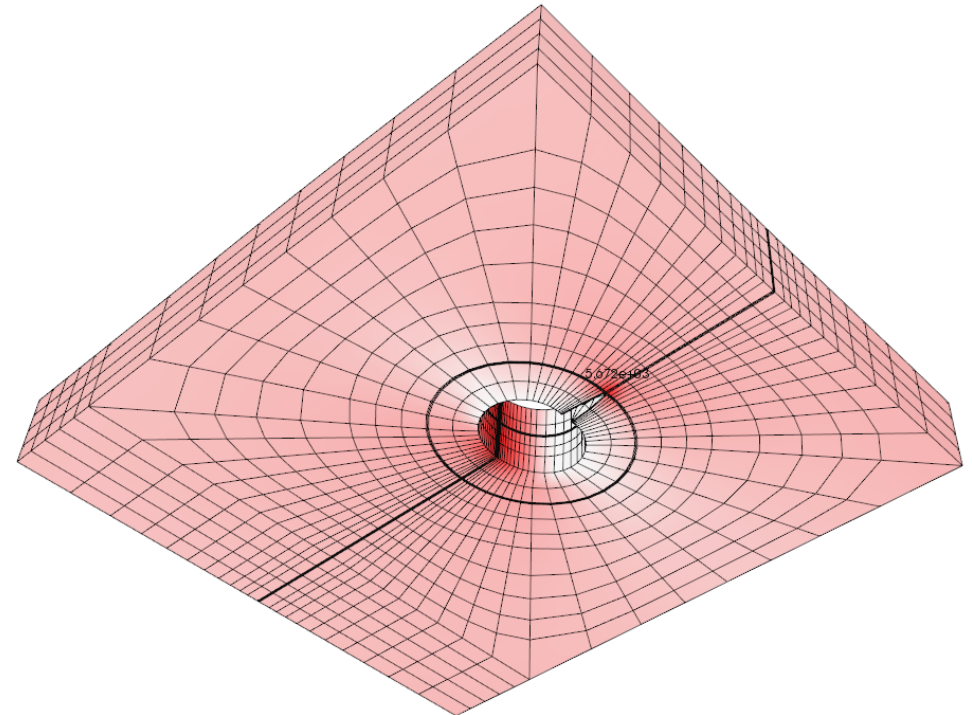
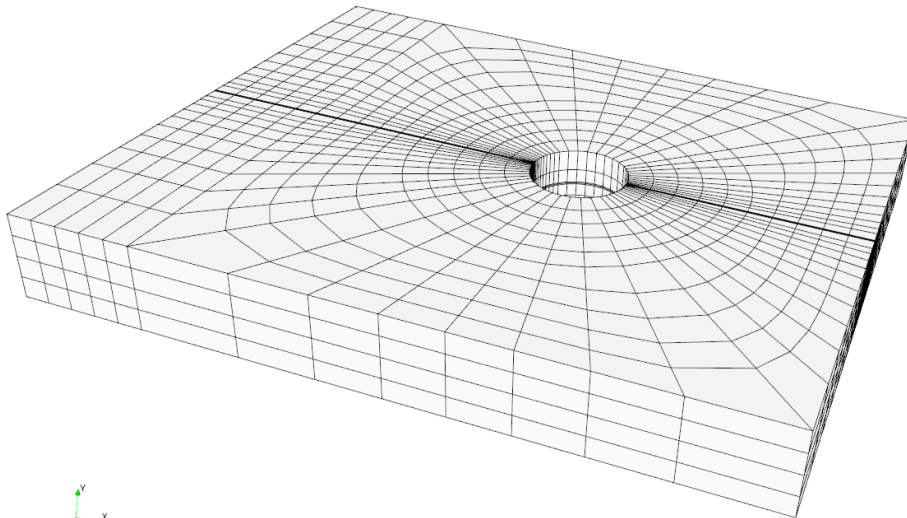
# QUICK2DFEM

- This capability allows immediate evaluation of Stress Concentration Factors in 2D models and F-DT analysis with the modules LIFING.LIFE or LIFING.GROWTH



# QUICK2DFEM

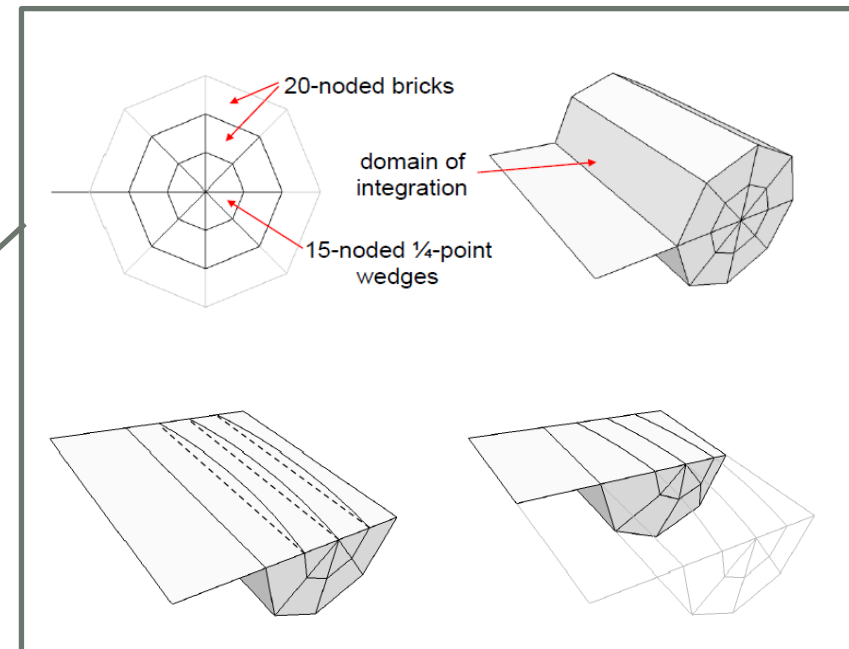
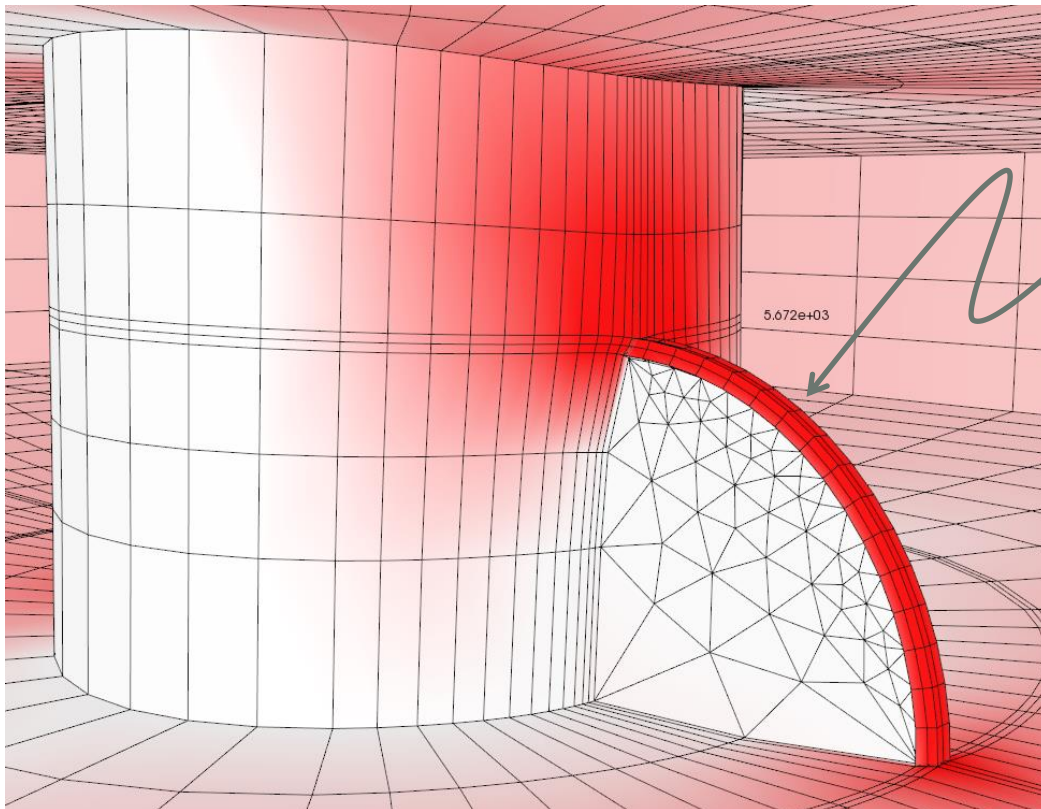
- With QUICK2DFEM it is possible to extrude linearly or circumferentially the generated 2D mesh, that can be solved with the internally coded 3D solver.
- A feature is implemented to introduce crack fronts.





# QUICK2DFEM

- The crack front is built with a template of elements, including quarter point elements, such to allow the M-Integral calculation and derivation of Stress Intensity Factors.



# TECHNICAL INFORMATION

- LIFING is developed by Fatigue Experts mainly operating in the Aerospace field, not just software developers, therefore implemented functionalities are effective for real life fatigue and damage tolerance analyses
- Parallel Processing is implemented (high performance)
- Graphics with VTK technology
- LIFING database consists of a generated SQLite database, easily readable and accessible with free packages (no need to keep the license to access, once expired, Fatigue calculation results)
- Results files are produced, such to allow the users to fully 'debug' their analysis
- Under constant improvement and upgrades
- For further info mail to: [support@lifing-fdt.com](mailto:support@lifing-fdt.com)

# REFERENCES



Tata Consultancy Services



Maserati



UNIVERSITÀ DEGLI STUDI DI PARMA

UniParma



Pilatus Aircraft



Aerea



Flowserve



Aquila Engineering



CST Firenze